

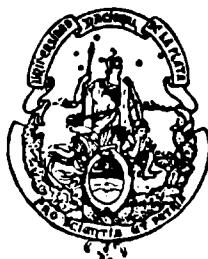
OBSERVATORIO ASTRONOMICO DE LA UNIVERSIDAD NACIONAL DE LA PLATA

SERIE ASTRONOMICA - Tomo XXIX₃

CORRECCIONES DE TRAZO
DEL CIRCULO II
DEL ANTEOJO MERIDIANO REPSOLD

P O R

SERGEJS J. SLAUCITAJS



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CORRECCIONES DE TRAZO DEL CIRCULO II DEL ANTEOJO MERIDIANO REPSOLD

Por el Dr. SERGEJS J. SLAUCITAJS(*)

1. — *Introducción.* Las correcciones para cada trazo del círculo II (sin freno) del anteojos meridiano Repsold fueron determinadas con los mismos métodos que para las del círculo I: c_x para grados enteros, con el método de rosetas (¹) y c_x de cuatro en cuatro minutos, con mediciones directas de intervalos (²) aprovechando las correcciones para grados enteros como datos de apoyo.

Para el cálculo de las correcciones de trazo de los grados enteros se utilizó el material de observación de las mediciones efectuadas en los años 1940 y 1941, completado en el año 1951. Las lecturas de los microscopios para la determinación de las correcciones de cada trazo fueron realizadas en los años 1951 y 1952.

Las correcciones de trazo provisorias, para grados enteros están publicadas en esta serie de publicaciones (³).

2. — *Correcciones de trazo grado por grado (diámetros).* a) *Resultados de las mediciones.* Las tablas I, II, III, IV, V, VI, VII (pág. 6-8) contienen los valores de A_x , B_x , C_x , D_x , E_x , F_x , G_x , H_x y J_x . La tabla VIII (pág. 9) — los valores de c_x para los 180 diámetros correspondientes, obtenidos directamente según la relación: $c_x = 1/18(G_x + 1/14H_x + 7/90J_x)$ (⁴).

b) *Correcciones a las lecturas de dos microscopios opuestos (c_x^2) y a los promedios de las lecturas de los cuatro microscopios que distan 90° (c_x^4).* Estas correcciones están dadas, hasta centésimos de segundo, en la tabla IX (pág. 10), despreciando los milésimos que no responden a una utilidad práctica (⁵).

(¹) BRUNS H., *Untersuchung einer Wannschaff'schen Theilung*, A. N. Bd. 130, Kiel, 1892.

(²) SLAUCITAJS S. J., *Correcciones de trazo del círculo I del anteojos meridiano Repsold*, Publ. del Obs. Astr. de la Universidad Nacional de La Plata, Serie Astronómica XXIX₂, La Plata, 1958.

(³) MARTÍNEZ H. A., *Catálogo de 3.710 estrellas galácticas australes*, Publ. del Obs. Astr. de la Universidad Nacional de La Plata, Serie Astronómica XIX, La Plata, 1943.

(⁴) Loc. cit. (³), Cap. II, 3.

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TABLA I

$$A_x = d_x^{36} + d_x^{72}; \quad B_x = d_x^{20} + d_x^{40} + d_x^{60} + d_x^{80}; \quad D_x = A_x + B_x$$

Los resultados están expresados en segundos de arco

<i>x</i>	<i>A_x</i>	<i>B_x</i>	<i>D_x</i>												
0°	— .030	— 1.520	— 1.550	45°	— 2.425	— 1.955	— 4.380	90°	— .120	+ 1.595	+ 1.475	135°	+ .445	+ 1.315	+ 1.760
1	— .980	— 1.815	— 2.795	46	— 1.850	— 1.395	— 3.245	91	— .590	— 2.590	— 3.180	136	+ 5.080	+ 1.460	+ 6.540
2	— 1.175	— 1.360	— 2.535	47	— 1.345	— 1.780	— 3.125	92	— 1.150	— 1.400	— 2.550	137	+ 6.690	+ 1.775	+ 8.465
3	— .835	+ .730	— .105	48	— .105	+ 4.015	+ 3.910	93	— 1.770	— 1.880	— 3.650	138	+ 3.725	+ .705	+ 4.430
4	— 1.305	— 2.160	— 3.465	49	+ .540	+ 4.940	+ 5.480	94	— 1.250	— 1.500	— 2.750	139	+ .155	+ .845	+ 1.000
5	— 1.135	+ .085	— 1.050	50	+ .595	+ 3.715	+ 4.310	95	— 2.205	— 3.320	— 5.525	140	+ .880	+ 2.895	+ 3.775
6	— .235	— .530	— .765	51	— .115	— 1.455	— 1.570	96	— 1.840	— 2.215	— 4.055	141	+ .970	+ 1.290	+ 2.260
7	— .020	— .245	— .265	52	+ .285	— 1.655	— 1.370	97	— 2.535	— 4.985	— 7.520	142	+ 1.760	+ 4.055	+ 5.815
8	+ 1.325	+ 5.975	+ 7.300	53	— .100	— 1.030	— 1.130	98	— .845	— 2.960	— 3.805	143	+ 1.455	+ .740	+ 2.195
9	+ .055	+ 5.145	+ 5.200	54	+ .255	— .560	— .305	99	— .030	— 1.400	— 1.430	144	+ 1.705	+ 1.655	+ 3.360
10	+ .075	+ 4.900	+ 4.975	55	+ .735	+ 1.005	+ 1.740	100	+ 4.035	— 1.390	+ 2.645	145	+ 1.300	+ 2.390	+ 3.690
11	— .540	— .965	— 1.505	56	+ .330	+ 2.640	+ 2.970	101	+ 4.365	— 1.620	+ 2.745	146	— .055	+ .870	+ .815
12	+ .310	+ .015	+ .325	57	+ 1.515	+ 3.155	+ 4.670	102	+ 2.315	— .920	+ 1.395	147	+ 1.015	+ 3.245	+ 4.260
13	— .260	— .415	— .675	58	+ 2.900	+ 4.120	+ 7.020	103	— 1.615	— 2.265	— 3.880	148	+ 1.825	+ 7.335	+ 9.160
14	+ .525	+ .160	+ .685	59	+ .410	+ 1.240	+ 1.650	104	— 1.630	— 2.175	— 3.805	149	+ 3.195	+ 12.070	+ 15.265
15	— .610	— 1.980	— 2.590	60	+ .935	+ 2.950	+ 3.885	105	— .130	— .865	— .995	150	+ .610	+ 5.570	+ 6.180
16	— .755	— 2.960	— 3.715	61	+ .765	+ 1.660	+ 2.425	106	— .630	— .485	— 1.115	151	+ .515	+ .930	+ 1.445
17	+ .285	— 1.425	— 1.140	62	+ .010	— .375	— .365	107	— .055	— 1.275	— 1.330	152	— .820	— .925	— 1.745
18	+ 1.020	— 1.595	— .575	63	+ 1.170	+ 1.865	+ 3.035	108	+ .825	+ 3.295	+ 4.120	153	+ .505	+ 1.105	+ 1.610
19	— .370	— .890	— 1.260	64	+ 5.165	+ .650	+ 5.815	109	+ .125	+ 4.105	+ 4.230	154	— .025	+ 1.500	+ 1.475
20	— .675	— .240	— .915	65	+ 5.145	— .600	+ 4.545	110	+ .680	+ 5.210	+ 5.890	155	+ 1.615	+ 4.110	+ 5.725
21	— .510	— 1.255	— 1.765	66	+ 3.230	+ .635	+ 3.865	111	+ 1.045	+ 2.885	+ 3.930	156	— .080	+ .705	+ .625
22	— .880	— 1.375	— 2.255	67	+ .940	+ 2.430	+ 3.370	112	+ .485	+ 1.140	+ 1.625	157	— .775	— 1.130	— 1.905
23	+ .605	+ 1.425	+ 2.030	68	+ .340	+ 5.105	+ 5.445	113	— .880	+ 1.385	+ .505	158	— .870	— 3.655	— 4.525
24	— .580	— .350	— .930	69	+ .395	+ 4.880	+ 5.275	114	— 1.325	— 1.385	— 2.710	159	+ .250	— 1.320	— 1.070
25	— .185	— .075	— .260	70	— .465	+ 2.195	+ 1.730	115	+ .395	+ 2.585	+ 2.980	160	+ .235	— 1.580	— 1.345
26	+ .680	+ .120	+ .800	71	+ 1.260	+ .045	+ 1.305	116	+ .560	+ 1.630	+ 2.190	161	+ .250	— .905	— .655
27	— 2.665	— 6.510	— 9.175	72	+ .590	— .645	— .055	117	+ 1.075	+ 2.380	+ 3.455	162	— .365	— 2.065	— 2.430
28	— 20.185	— 40.230	— 60.415	73	+ .485	+ .940	+ 1.425	118	+ .165	+ .450	+ .615	163	+ .275	+ .560	+ .835
29	— 22.750	— 46.755	— 69.505	74	+ .290	+ 1.970	+ 2.260	119	— .585	+ .145	+ .440	164	+ 1.785	+ 4.565	+ 6.350
30	— 13.115	— 26.700	— 39.815	75	+ .700	+ 3.620	+ 4.320	120	+ .365	+ 1.275	+ 1.640	165	+ .890	+ 2.405	+ 3.295
31	— .125	— .320	— .445	76	+ 1.520	+ 3.735	+ 5.255	121	+ .035	+ .670	+ .705	166	+ 1.295	+ 2.055	+ 3.350
32	— .555	— .930	— 1.485	77	+ 1.005	+ 3.220	+ 4.225	122	— .545	— 1.020	— 1.565	167	+ 1.140	+ 2.335	+ 3.475
33	— 1.505	— 3.105	— 4.610	78	+ 2.470	+ 3.835	+ 6.305	123	— 1.150	— 2.345	— 3.495	168	+ 1.245	+ 6.735	+ 7.980
34	— .970	— 2.210	— 3.180	79	+ 1.770	+ 3.320	+ 5.090	124	+ .360	+ .375	+ .735	169	+ 1.705	+ 6.935	+ 8.640
35	— 4.115	— 9.270	— 13.385	80	+ .630	+ 1.980	+ 2.610	125	— 1.345	— 3.425	— 4.770	170	+ .525	+ 3.690	+ 4.215
36	— 3.090	— 7.350	— 10.440	81	+ .790	+ 3.370	+ 4.160	126	— .790	— 2.170	— 2.960	171	+ 1.080	+ .915	+ 1.995
37	— .930	— 2.550	— 3.480	82	+ 1.635	+ 4.710	+ 6.345	127	— .050	— .580	— .630	172	+ 5.905	+ 3.155	+ 9.060
38	+ .260	— .030	+ .230	83	+ .855	+ 3.070	+ 3.925	128	— .290	+ 5.220	+ 4.930	173	+ 6.550	+ 1.695	+ 8.245
39	— 1.925	— 2.230	— 4.155	84	— .490	— .625	— 1.115	129	— .125	+ 4.265	+ 4.140	174	+ 3.845	+ 1.830	+ 5.675
40	— 2.525	— 4.370	— 6.895	85	+ .460	+ 2.040	+ 2.500	130	— 2.065	— .175	— 2.240	175	+ .645	+ 1.935	+ 2.580
41	— 2.185	— 1.395	— 3.580	86	+ .295	+ .900	+ 1.195	131	+ .050	+ .555	+ .605	176	+ .965	+ 2.355	+ 3.320
42	— 1.520	— 1.650	— 3.170	87	+ 1.625	+ 2.380	+ 4.005	132	+ .240	+ 1.245	+ 1.485	177	+ .270	— .440	— .170
43	— 2.660	— 3.780	— 6.440	88	— .125	+ 2.550	+ 2.425	133	+ .250	+ 1.305	+ 1.555	178	+ .305	— .870	— .565
44	— 1.695	— 1.935	— 3.630	89	+ .910	+ 4.415	+ 5.325	134	— .370	+ .195	— .175	179	+ 1.455	+ .290	+ 1.745

TABLA II

$$C_x = d_x^{45} + \frac{1}{2} d_x^{90}$$

Los resultados están expresados en segundos de arco

x	C_x	x	C_x	x	C_x	x	C_x
0°	— .160	45°	— .700	90°	— .090	135°	+ .950
1	— .278	46	— .845	91	— .142	136	+ 1.265
2	— .460	47	— .960	92	— .300	137	+ 1.720
3	+ .280	48	+ .455	93	— 1.300	138	+ .565
4	— .760	49	+ .330	94	— .640	139	+ 1.070
5	— .082	50	+ .300	95	— 2.108	140	+ 1.890
6	+ .565	51	— .310	96	— 1.125	141	+ .870
7	+ .720	52	+ .185	97	— 2.220	142	+ 1.315
8	+ 1.350	53	+ .030	98	— 1.310	143	— .070
9	+ 1.965	54	— .880	99	— 1.885	144	+ .800
10	+ .335	55	+ .555	100	— .945	145	+ .055
11	+ .065	56	+ .320	101	— .835	146	+ .450
12	— .850	57	+ 1.670	102	— 1.360	147	+ .540
13	— .875	58	+ 1.760	103	— 1.815	148	+ .930
14	+ .615	59	— 1.350	104	— 1.805	149	+ 2.540
15	— 1.070	60	+ 1.355	105	— .690	150	+ .405
16	— 1.605	61	+ .470	106	— .005	151	+ 1.140
17	— .205	62	— .155	107	— .055	152	+ .415
18	— .260	63	+ .240	108	— .790	153	+ .810
19	— .620	64	+ .760	109	— .640	154	+ .500
20	— .235	65	— 1.290	110	— .085	155	+ 1.610
21	— .395	66	— .500	111	+ .795	156	+ .100
22	— .320	67	+ .530	112	— .090	157	— .120
23	+ .725	68	+ .530	113	+ .135	158	— 1.390
24	+ .800	69	— .095	114	— .800	159	+ .095
25	+ .455	70	+ .040	115	+ .865	160	— 1.360
26	+ .040	71	— .070	116	+ .500	161	— .470
27	— 1.870	72	+ .660	117	+ 2.210	162	— 1.000
28	— 14.325	73	+ 4.430	118	+ 5.245	163	+ 4.650
29	— 17.525	74	+ 5.800	119	+ 5.035	164	+ 6.690
30	— 10.515	75	+ 4.085	120	+ 3.235	165	+ 3.195
31	— .625	76	+ .515	121	— .215	166	+ .325
32	— 1.185	77	+ 1.600	122	— .815	167	+ .400
33	— 1.175	78	+ 1.825	123	— 1.675	168	+ 1.025
34	— 1.510	79	+ .870	124	— .340	169	+ .980
35	— 2.755	80	+ 1.765	125	— .165	170	+ 1.155
36	— 2.100	81	+ 1.890	126	— .550	171	+ .760
37	— 1.705	82	+ 1.495	127	— .955	172	+ 1.165
38	+ .050	83	+ .340	128	— .840	173	+ .450
39	— .370	84	— .200	129	— .010	174	+ .580
40	— 1.075	85	+ 1.040	130	— .485	175	+ .520
41	— .560	86	— .265	131	+ .850	176	— .025
42	— 1.225	87	+ .940	132	+ .805	177	— .520
43	— 1.360	88	— .645	133	+ 1.230	178	+ .775
44	— .930	89	+ .080	134	+ .210	179	+ .640

TABLA III

$$E_x = D_x + D_{x+36} + \\ + D_{x+72} + D_{x+108} + \\ + D_{x+144}$$

TABLA IV

$$F_x = D_x + D_{x+20} + D_{x+40} + \\ + D_{x+60} + D_{x+80} + D_{x+100} + \\ + D_{x+120} + D_{x+140} + D_{x+160}$$

TABLA V

$$G_x = C_x + D_x + \frac{1}{9} E_x + \frac{1}{5} F_x$$

Los resultados están expresados en segundos de arco

x	G_x	x	G_x	x	G_x	x	G_x
0°	— 1.447	45°	— 3.449	90°	— 1.804	135°	+ 1.807
1	— 2.032	46	— 2.572	91	— 3.083	136	+ 4.304
2	— 2.008	47	— 3.459	92	— .594	137	+ 6.449
3	+ .712	48	+ 1.934	93	— 3.552	138	+ 4.104
4	— 2.931	49	+ 3.298	94	— 2.848	139	+ 2.588
5	+ 1.090	50	+ 1.965	95	— 7.864	140	+ 7.241
6	+ .837	51	— 1.888	96	— 3.713	141	+ 4.026
7	+ .884	52	— .490	97	— 7.882	142	+ 7.675
8	+ 6.368	53	— .708	98	— 3.215	143	+ .693
9	+ 5.091	54	— 1.523	99	— 3.513	144	+ 4.316
10	+ 3.784	55	+ 1.539	100	— 1.569	145	+ 4.601
11	— .415	56	+ 5.026	101	— 2.446	146	+ 2.393
12	+ 1.131	57	+ 8.403	102	— 2.435	147	+ 5.834
13	— .217	58	+ 10.953	103	— 5.783	148	+ 7.692
14	+ 1.506	59	+ .774	104	— 4.141	149	+ 16.322
15	— 4.663	60	+ 6.939	105	— .974	150	+ 4.578
16	— 5.145	61	+ 4.133	106	— .434	151	+ 3.413
17	— .288	62	— .199	107	— 2.320	152	+ .475
18	+ .458	63	+ 2.471	108	— .206	153	+ 4.191
19	— 1.931	64	+ 3.199	109	+ .741	154	+ 3.300
20	+ .818	65	— 1.286	110	+ 3.889	155	+ 7.365
21	— .717	66	+ 1.036	111	+ 6.158	156	+ 1.861
22	— 1.981	67	+ 4.309	112	+ 3.224	157	— .027
23	+ 2.623	68	+ 3.752	113	+ 3.002	158	— 4.078
24	+ 1.462	69	+ 2.186	114	— 2.666	159	— 1.273
25	+ 1.248	70	— .588	115	+ 3.678	160	— 2.298
26	+ 1.302	71	+ .699	116	+ 3.975	161	— .688
27	— 11.352	72	+ 1.156	117	+ 8.101	162	— 3.716
28	— 81.808	73	+ 6.851	118	+ 8.816	163	+ 4.828
29	— 95.276	74	+ 8.995	119	+ 5.330	164	+ 14.901
30	— 55.703	75	+ 8.843	120	+ 6.243	165	+ 7.748
31	— .262	76	+ 6.939	121	+ 1.868	166	+ 4.410
32	— .806	77	+ 8.852	122	— 2.122	167	+ 4.240
33	— 4.934	78	+ 10.605	123	— 6.074	168	+ 6.905
34	— 4.197	79	+ 6.498	124	+ .695	169	+ 6.968
35	— 17.671	80	+ 5.892	125	— 4.683	170	+ 2.788
36	— 12.509	81	+ 7.866	126	— 3.655	171	+ 2.847
37	— 3.524	82	+ 9.217	127	— 1.745	172	+ 7.244
38	+ 2.846	83	+ 4.394	128	+ 2.259	173	+ 4.294
39	— 3.382	84	— .054	129	+ 1.683	174	+ 3.733
40	— 6.569	85	+ 4.733	130	— 5.034	175	+ 2.913
41	— 1.733	86	+ 1.329	131	+ 2.219	176	+ 4.639
42	— 3.499	87	+ 4.538	132	+ 4.277	177	+ .826
43	— 7.868	88	— 1.612	133	+ 3.978	178	+ 2.334
44	— 3.150	89	+ 1.952	134	+ .304	179	+ 1.559

TABLA VI

$$H_x = G_x + G_{x+45} + \\ + G_{x+90} + G_{x+135}$$

Los resultados están expresados en segundos de arco

x	H_x
0°	— 4.893
1	— 3.383
2	+ .388
3	+ 3.198
4	+ .107
5	+ 2.432
6	— .738
7	+ .187
8	+ 3.138
9	+ 4.371
10	+ 8.355
11	+ 4.558
12	+ 12.933
13	+ 12.645
14	+ 14.461
15	+ 5.880
16	+ 1.967
17	— 2.332
18	+ 6.914
19	+ 5.309
20	+ 10.786
21	+ 8.338
22	+ 5.525
23	+ 5.299
24	— .291
25	+ 2.040
26	+ 5.288
27	— 5.811
28	— 61.313
29	— 66.050
30	— 32.869
31	+ 12.955
32	+ 10.164
33	+ 6.502
34	+ 9.964
35	— 13.671
36	— 5.451
37	+ 11.192
38	+ 13.793
39	+ 1.980
40	— 3.957
41	+ 6.454
42	+ 6.142
43	— 3.168
44	+ .665

TABLA VII

$$J_x = G_x + G_{x+45} + \\ + G_{x+90} + \dots + G_{x+170}$$

TABLA VIII

Los resultados están expresados en segundos de arco

x	C_x	x	C_x	x	C_x	x	C_x
0°	— 0.118	45°	— .228	90°	— .124	135°	+ .121
1	— .143	46	— .161	91	— .145	136	+ .208
2	— .115	47	— .151	92	— .050	137	+ .343
3	+ .092	48	+ .102	93	— .202	138	+ .236
4	— .180	49	+ .167	94	— .163	139	+ .184
5	+ .053	50	+ .114	95	— .387	140	+ .394
6	+ .039	51	— .062	96	— .227	141	+ .204
7	+ .090	52	— .045	97	— .454	142	+ .422
8	+ .348	53	— .041	98	— .171	143	+ .091
9	+ .283	54	— .072	99	— .138	144	+ .239
10	+ .239	55	+ .158	100	— .072	145	+ .272
11	+ .035	56	+ .279	101	— .135	146	+ .146
12	+ .096	57	+ .501	102	— .089	147	+ .415
13	+ .021	58	+ .654	103	— .231	148	+ .459
14	+ .136	59	+ .140	104	— .191	149	+ .947
15	— .196	60	+ .391	105	— .048	150	+ .273
16	— .296	61	+ .221	106	— .021	151	+ .237
17	— .042	62	— .025	107	— .098	152	— .001
18	+ .048	63	+ .204	108	— .002	153	+ .243
19	— .046	64	+ .181	109	+ .045	154	+ .200
20	+ .070	65	— .046	110	+ .254	155	+ .492
21	— .024	66	+ .086	111	+ .415	156	+ .118
22	— .093	67	+ .301	112	+ .183	157	+ .004
23	+ .206	68	+ .211	113	+ .171	158	— .210
24	+ .062	69	+ .103	114	— .154	159	— .032
25	+ .061	70	— .029	115	+ .252	160	— .138
26	+ .088	71	+ .100	116	+ .224	161	— .034
27	— .614	72	+ .023	117	+ .410	162	— .234
28	— 4.806	73	+ .120	118	+ .242	163	+ .065
29	— 5.572	74	+ .233	119	+ .074	164	+ .548
30	— 3.230	75	+ .401	120	+ .198	165	+ .283
31	+ .077	76	+ .419	121	+ .138	166	+ .292
32	— .022	77	+ .515	122	— .082	167	+ .316
33	— .265	78	+ .610	123	— .272	168	+ .391
34	— .198	79	+ .440	124	+ .060	169	+ .410
35	— .996	80	+ .255	125	— .331	170	+ .096
36	— .735	81	+ .398	126	— .230	171	+ .176
37	— .168	82	+ .552	127	— .013	172	+ .429
38	+ .208	83	+ .339	128	+ .162	173	+ .276
39	— .140	84	— .013	129	+ .084	174	+ .210
40	— .399	85	+ .230	130	— .300	175	+ .186
41	— .088	86	+ .095	131	+ .189	176	+ .265
42	— .175	87	+ .316	132	+ .244	177	+ .053
43	— .410	88	— .120	133	+ .192	178	+ .112
44	— .190	89	+ .094	134	+ .015	179	+ .129

De la tabla VIII se ve, que el círculo tiene para $x = 27, 28, 29, 30, 35, 36, (38)$ y 149 errores de graduación groseros. Excluyendo los trazos mencionados de la suma $c_x + c_x + 4 + c_x + 8 + \dots = 0$, hemos corregido los valores, dados en la misma, con las magnitudes:

$$c_0 + 4_n : - 0''123$$

$$c_1 + 4_n : - .103$$

$$c_2 + 4_n : - .067$$

$$c_3 + 4_n : - .036, n = 0, 1, 2, \dots, 44.$$

La tabla IX contiene los valores de c_x^2 y c_x^4 adoptados como definitivos.

TABLA IX

Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4
0° 180°	— 0''24	90° 270°	— 0''19	0° 90° 180° 270°	— 0''22
1	— .25	91	— .18	1	— .22
2	— .18	92	— .17	2	— .18
3	+ .05	93	— .31	3	— .12
4	— .30	94	— .23	4	— .27
5 185	— .05	95 275	— .42	5 95 185 275	— .23
6	— .03	96	— .35	6	— .19
7	+ .05	97	— .56	7	— .25
8	+ .23	98	— .24	8	— .01
9	+ .18	99	— .17	9	± .00
10 190	+ .17	100 280	— .20	10 100 190 280	— .01
11	± .00	101	— .24	11	— .12
12	— .03	102	— .15	12	— .09
13	— .08	103	— .27	13	— .18
14	+ .07	104	— .31	14	— .12
15 195	— .23	105 285	— .15	15 105 195 285	— .19
16	— .42	106	— .09	16	— .25
17	— .15	107	— .13	17	— .14
18	— .02	108	— .12	18	— .07
19	— .08	109	— .06	19	— .07
20 200	— .05	110 290	+ .19	20 110 200 290	+ .07
21	— .13	111	+ .38	21	+ .13
22	— .16	112	+ .06	22	— .05
23	+ .17	113	+ .07	23	+ .12
24	— .06	114	— .22	24	— .14
25 205	— .04	115 295	+ .22	25 115 205 295	+ .09
26	+ .02	116	+ .10	26	+ .06
27	— 0.65	117	+ .31	27	— 0.17
28	— 4.93	118	+ .18	28	— 2.38
29	— 5.68	119	+ .04	29	— 2.82
30 210	— 3.30	120 300	— .08	30 120 210 300	— 1.61
31	+ 0.04	121	+ .04	31	+ 0.04
32	— .15	122	— .15	32	— .15
33	— .37	123	— .31	33	— .34
34	— .27	124	— .06	34	— .17
35 215	— 1.03	125 305	— .43	35 125 215 305	— .73
36	— 0.86	126	— .30	36	— .58
37	— .27	127	— .05	37	— .16
38	+ .14	128	+ .04	38	+ .09
39	— .18	129	— .02	39	— .10
40 220	— .52	130 310	— .37	40 130 220 310	— .44
41	— .19	131	+ .15	41	— .02
42	— .24	132	+ .12	42	— .06
43	— .45	133	+ .09	43	— .18
44	— .31	134	— .05	44	— .18
45° 225°	— 0''33	135° 315°	+ 0''08	45° 135° 225° 315°	— 0''12
46	— .23	136	+ .09	46	+ .07
47	— .19	137	+ .24	47	+ .03
48	— .02	138	+ .17	48	+ .07
49	+ .06	139	+ .15	49	+ .11
50 230	+ .05	140 320	+ .27	50 140 230 320	+ .16
51	— .10	141	+ .10	51	± .00
52	— .17	142	+ .36	52	+ .09
53	— .15	143	+ .06	53	— .05
54	— .14	144	+ .12	54	— .01

TABLA IX (continuación)

Trazos		c_x^2	Trazos		c_x^2	Trazos				c_x^4
55	235	— .12	145	325	+ .17	55	145	235	325	+ .14
56		+ .16	146		+ .08	56				+ .12
57		+ .40	147		+ .38	57				+ .39
58		+ .59	148		+ .34	58				+ .46
59		+ .10	149		+ .84	59				+ .47
60	240	+ .27	150	330	+ .21	60	150	240	330	+ .24
61		+ .12	151		+ .20	61				+ .16
62		— .09	152		— .12	62				— .11
63		+ .17	153		+ .14	63				+ .15
64		+ .06	154		+ .13	64				+ .10
65	245	— .15	155	335	+ .46	65	155	245	335	+ .15
66		+ .02	156		± .00	66				+ .01
67		+ .26	157		— .10	67				+ .08
68		+ .09	158		— .28	68				— .09
69		± .00	159		— .07	69				— .03
70	250	— .10	160	340	— .26	70	160	250	340	— .18
71		+ .06	161		— .14	71				— .04
72		— .10	162		— .30	72				— .20
73		+ .02	163		+ .03	73				+ .02
74		+ .17	164		+ .42	74				+ .30
75	255	+ .36	165	345	+ .18	75	165	255	345	+ .27
76		+ .30	166		+ .22	76				+ .26
77		+ .41	167		+ .28	77				+ .34
78		+ .54	168		+ .27	78				+ .41
79		+ .40	169		+ .31	79				+ .36
80	260	+ .13	170	350	+ .03	80	170	260	350	+ .08
81		+ .30	171		+ .14	81				+ .22
82		+ .48	172		+ .31	82				+ .40
83		+ .30	173		+ .17	83				+ .24
84		— .14	174		+ .14	84				± .00
85	265	+ .13	175	355	+ .15	85	175	265	355	+ .14
86		+ .03	176		+ .15	86				+ .08
87		+ .28	177		— .05	87				+ .12
88		— .24	178		+ .04	88				— .10
89		— .01	179		+ .09	89				+ .04

3. — *Representación de las correcciones de trazo para grados enteros por medio de la serie de Fourier.* La representación de c_x^4 por medio de la serie de Fourier da:

$$c_x^4 = + 0.144 \operatorname{sen}(179^\circ 9 + x) + 0.040 \operatorname{sen}(258^\circ 6 + 2x) + 0.118 \operatorname{sen}(181^\circ 2 + 3x) + 0.070 \operatorname{sen}(245^\circ 5 + 4x) + \\ + 0.070 \operatorname{sen}(308^\circ 2 + 5x) + 0.011 \operatorname{sen}(173^\circ 5 + 6x) + \dots + \sigma_i.$$

El valor medio σ de σ_i , tomando en cuenta los primeros k -términos de la serie:

$$k = \begin{matrix} 1 & 2 & 3 & 4 & 5 & 6 \end{matrix}$$

$$\sigma = \pm 0''15_0 \pm 0''15_7 \pm 0''09_5 \pm 0''08_1 \pm 0''06_1 \pm 0''06_2$$

La curva dibujada en la figura 1 representa el resultado de la suma de los seis primeros términos de la serie.

En la tabla X, siguiente, están dados los valores $0-C$, los residuos entre los valores observados de $c_x^4(0)$ y los que resultan de los seis primeros términos del desarrollo en serie de Fourier, curva (C).

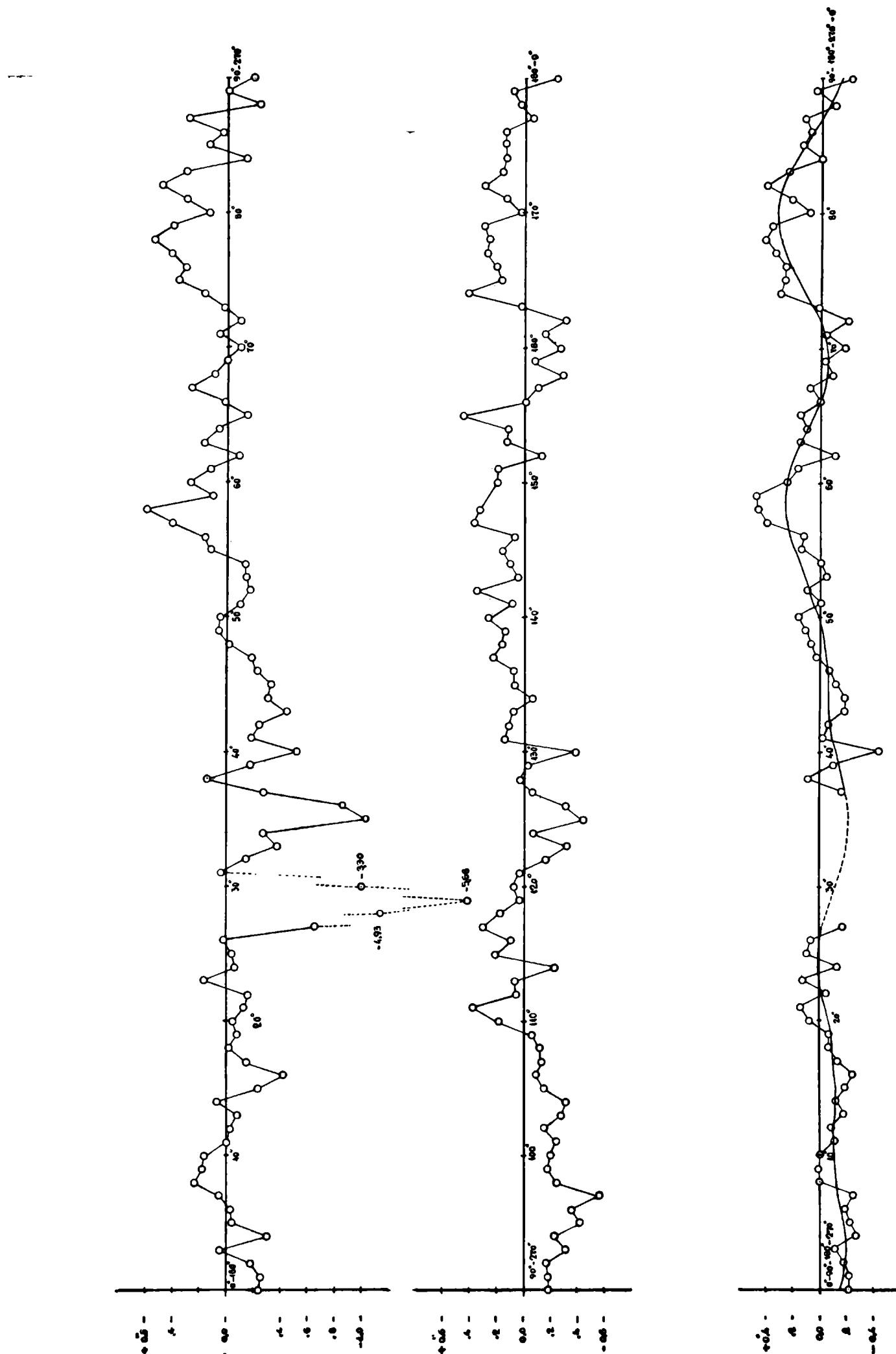


TABLA X

Trazos				C	O-C	Trazos				C	O-C
0°	90°	180°	270°	— "15	— "07	45°	135°	225°	315°	— "06	— "06
1				— .18	— .04	46				— .05	— .02
2				— .19	+ .01	47				— .04	+ .07
3				— .20	+ .08	48				— .03	+ .10
4				— .19	— .08	49				— .02	+ .13
5	95	185	275	— .18	— .05	50	140	230	320	+ .01	+ .15
6				— .16	— .03	51				+ .04	— .04
7				— .14	— .11	52				+ .07	+ .02
8				— .13	+ .12	53				+ .11	— .16
9				— .12	+ .12	54				+ .15	— .16
10	100	190	280	— .11	+ .10	55	145	235	325	+ .19	— .05
11				— .10	— .02	56				+ .22	— .10
12				— .10	+ .01	57				+ .25	+ .14
13				— .11	— .07	58				+ .27	+ .19
14				— .11	— .01	59				+ .27	+ .20
15	105	195	285	— .12	— .07	60	150	240	330	+ .26	— .02
16				— .10	— .15	61				+ .24	— .08
17				— .10	— .04	62				+ .20	— .31
18				— .09	+ .02	63				+ .14	+ .01
19				— .08	+ .01	64				+ .10	± .00
20	110	200	290	— .06	+ .13	65	155	245	335	+ .05	+ .10
21				— .04	+ .17	66				± .00	+ .01
22				— .02	— .03	67				— .03	+ .11
23				— .00	+ .12	68				— .05	— .04
24				+ .01	— .15	69				— .06	+ .03
25	115	205	295	+ .01	+ .08	70	160	250	340	— .05	— .13
26				— .00	+ .06	71				— .02	— .02
27				— .02	— .15	72				+ .02	— .22
28				(— .04)	(— 2.34)	73				+ .05	— .03
29				(— .07)	(— 2.75)	74				+ .11	+ .19
30	120	210	300	(— .10)	(— 1.51)	75	165	255	345	+ .17	+ .10
31				(— .14)	(+ .18)	76				+ .23	+ .03
32				(— .17)	(+ .02)	77				+ .27	+ .07
33				(— .19)	(— .15)	78				+ .30	+ .11
34				(— .20)	(+ .03)	79				+ .32	+ .03
35	125	215	305	(— .21)	(— .52)	80	170	260	350	+ .34	— .26
36				(— .20)	(— .38)	81				+ .31	— .09
37				— .19	+ .03	82				+ .29	+ .11
38				— .17	+ .26	83				+ .24	± .00
39				— .15	+ .05	84				+ .19	— .19
40	130	220	310	— .12	— .32	85	175	265	355	+ .12	+ .01
41				— .09	+ .07	86				+ .06	+ .02
42				— .07	+ .01	87				— .00	+ .12
43				— .07	— .11	88				— .06	— .04
44				— .06	— .12	89				— .11	+ .15

4.— *Correcciones de trazo de cuatro en cuatro minutos (diámetros).* Se elaboraron en la misma forma que para el círculo I⁽⁵⁾.

La tabla XI contiene las correcciones c_x^2 y c_x^4 para trazos de $4'$ en $4'$.

Las correcciones están dadas hasta centésimos de segundo.

⁽⁵⁾ Loc. cit.^a), Cap. III, 1.

TABLA XI

Los resultados están expresados en segundos de arco.

Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4	Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4
0°-180°-0'	- 0.24	90°-270°-0'	- 0.19	0°-90°-180°-270°-0'	- 0.22	4°-184°-0'	- 0.30	94°-274°-0'	- 0.23	4°-94°-184°-274°-0'	- .27
4' - .41		4' - .56		4' - .48		4' - .03		4' - .61		4' - .32	
8' + .18		8' - .23		8' - .02		8' - .28		8' - .36		8' - .32	
12' .00		12' - .30		12' - .15		12' - .30		12' - .68		12' - .49	
16' - .49		16' - .08		16' - .28		16' - .22		16' - .84		16' - .53	
20' - .27		20' + .06		20' - .10		20' - .74		20' - .88		20' - .81	
24' - .48		24' + .04		24' - .22		24' - .68		24' - .82		24' - .75	
28' - .58		28' - .38		28' - .48		28' - .76		28' - .71		28' - .74	
32' - .78		32' - .10		32' - .44		32' - .79		32' - .80		32' - .80	
36' - .70		36' - .11		36' - .40		36' - .81		36' - .56		36' - .68	
40' - .64		40' - .06		40' - .35		40' - 1.29		40' - 0.72		40' - 1.00	
44' - .74		44' + .08		44' - .33		44' - .88		44' - .68		44' - .78	
48' - .86		48' + .06		48' - .40		48' - .91		48' - .78		48' - .84	
52' - .72		52' - .01		52' - .36		52' - 1.28		52' - .92		52' - 1.10	
56' - .71		56' - .09		56' - .40		56' - 1.05		56' - .64		56' - .84	
1°-181°-0'	- 0.25	91°-271°-0'	- .18	1°-91°-181°-271°-0'	- .22	5°-185°-0'	- 0.05	95°-275°-0'	- 0.42	5°-95°-185°-275°-0'	- .23
4' - .32		4' - .20		4' - .26		4' - .42		4' - .46		4' - .44	
8' - .30		8' - .14		8' - .22		8' - .44		8' - .33		8' - .38	
12' - .38		12' - .22		12' - .30		12' - .62		12' - .58		12' - .60	
16' - .54		16' - .24		16' - .39		16' - .48		16' - .38		16' - .43	
20' - .14		20' - .24		20' - .19		20' - 0.66		20' - 0.44		20' - 0.55	
24' - .18		24' - .22		24' - .20		24' - .58		24' - .66		24' - .62	
28' - .02		28' - .06		28' - .04		28' - .65		28' - .58		28' - .62	
32' - .22		32' + .24		32' + .01		32' - .84		32' - .80		32' - .82	
36' + .08		36' - .04		36' + .02		36' - .60		36' - 1.40		36' - 1.00	
40' + .03		40' - .07		40' - .02		40' - 0.33		40' - 0.68		40' - 0.50	
44' - .19		44' + .08		44' - .06		44' - .47		44' - 1.04		44' - .76	
48' - .40		48' - .58		48' - .49		48' - .10		48' - .86		48' - .48	
52' - .68		52' + .11		52' - .28		52' - .25		52' - .80		52' - .52	
56' - .48		56' - .37		56' - .42		56' - .44		56' - .64		56' - .54	
2°-182°-0'	- .18	92°-272°-0'	- .17	2°-92°-182°-272°-0'	- .18	6°-186°-0'	- 0.03	96°-276°-0'	- 0.35	6°-96°-186°-276°-0'	- 0.19
4' - .52		4' - .44		4' - .48		4' - .36		4' - .68		4' - .52	
8' - .32		8' - .30		8' - .31		8' - .56		8' - .92		8' - .74	
12' - .31		12' - .88		12' - .60		12' - .54		12' - .70		12' - .62	
16' - .78		16' - .89		16' - .84		16' - .28		16' - .80		16' - .54	
20' - .77		20' - .65		20' - .71		20' - 0.16		20' - 0.74		20' - 0.45	
24' - .74		24' - .55		24' - .64		24' - .62		24' - .65		24' - .64	
28' - .80		28' - .20		28' - .50		28' - .14		28' - .92		28' - .53	
32' - .55		32' - .18		32' - .36		32' - .18		32' - .80		32' - .49	
36' - .40		36' - .00		36' - .20		36' - .52		36' - .94		36' - .73	
40' - .46		40' - .24		40' - .35		40' - 0.48		40' - 0.79		40' - 0.64	
44' - .64		44' - .30		44' - .47		44' - .49		44' - .63		44' - .56	
48' - .26		48' - .48		48' - .37		48' + .01		48' - .03		48' - .01	
52' - .44		52' - .37		52' - .40		52' + .10		52' - .18		52' - .04	
56' - .55		56' - .18		56' - .36		56' - 00		56' - .37		56' - .18	
3°-183°-0'	+ 0.05	93°-273°-0'	- .31	3°-93°-183°-273°-0'	- .12	7°-187°-0'	+ 0.05	97°-277°-0'	- 0.56	7°-97°-187°-277°-0'	- 0.25
4' - .24		4' - .03		4' - .14		4' + .28		4' - .10		4' + .09	
8' + .22		8' - .20		8' + .01		8' + .52		8' - .28		8' + .12	
12' - .44		12' + .11		12' - .16		12' + .42		12' - .06		12' + .18	
16' - .62		16' + .28		16' - .17		16' + .16		16' - .32		16' - .08	
20' - 0.02		20' + 0.61		20' + 0.30		20' + 0.30		20' - 0.22		20' + 0.04	
24' + .09		24' - 00		24' + .04		24' + .12		24' - .02		24' + .05	
28' + .44		28' + .40		28' + .42		28' + .56		28' - .33		28' + .12	
32' - .23		32' + .27		32' + .02		32' + .02		32' - .16		32' - .07	
36' + .05		36' + .38		36' + .22		36' + .28		36' - .17		36' + .06	
40' - .34		40' + .13		40' - .10		40' - 0.04		40' - 0.16		40' - .10	
44' + .12		44' - .08		44' + .02		44' + .28		44' - .30		44' - .01	
48' - .23		48' - .06		48' - .14		48' - .38		48' - .46		48' - .42	
52' - .00		52' - .32		52' - .16		52' - 00		52' - .68		52' - .34	
56' - .34		56' - .20		56' - .27		56' + .17		56' - .46		56' - .14	

Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4	Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4
8°-188°-0'	+ 0.23	98°-278°-0'	- 0.24	8°-98°-188°-278°-0'	- .01	12°-192°-0'	- 0.03	102°-282°-0'	- 0.15	12°-102°-192°-282°-0'	- 0.09
4' - .29		4' - .00		4' - .14		4' - .10		4' - .28		4' - .19	
8' - .16		8' + .09		8' - .04		8' - .10		8' - .28		8' - .19	
12' - .19		12' + .40		12' + .10		12' - .27		12' - .30		12' - .28	
16' + .29		16' + .34		16' + .32		16' - .24		16' + .14		16' - .05	
20' + 0.02		20' + 0.48		20' + 0.25		20' - 0.18		20' - 0.18		20' - 0.18	
24' + .36		24' + .22		24' + .29		24' - .64		24' + .24		24' - .20	
28' + .18		28' + .40		28' + .29		28' - .51		28' + .14		28' - .18	
32' + .35		32' + .18		32' + .26		32' - .48		32' + .38		32' - .05	
36' + .10		36' + .41		36' + .26		36' + .05		36' + .11		36' + .08	
40' + 0.33		40' + 0.28		40' + .30		40' + .20		40' + 0.14		40' + 0.17	
44' + .46		44' + .05		44' + .26		44' - .28		44' - .06		44' - .17	
48' + .76		48' - .02		48' + .37		48' + .13		48' - .01		48' + .06	
52' + .31		52' + .14		52' + .22		52' + .22		52' - .16		52' + .03	
56' + .29		56' + .05		56' + .17		56' - .26		56' - .46		56' - .36	
9°-189°-0'	+ 0.18	99°-279°-0'	- 0.17	9°-99°-189°-279°-0'	0.00	13°-193°-0'	- .08	103°-283°-0'	- 0.27	13°-103°-193°-283°-0'	- 0.18
4' + .38		4' - .08		4' + .15		4' - .14		4' - .19		4' - .16	
8' + .10		8' - .22		8' - .06		8' - .16		8' - .21		8' - .18	
12' + .15		12' - .41		12' - .13		12' - .24		12' - .20		12' - .22	
16' + .17		16' - .24		16' - .04		16' - .08		16' - .22		16' - .15	
20' + 0.36		20' - 0.26		20' + 0.05		20' + 0.14		20' - 0.36		20' - 0.11	
24' + .10		24' + .05		24' + .08		24' - .02		24' - .49		24' - .26	
28' - .04		28' - .30		28' - .17		28' + .11		28' - .84		28' - .36	
32' - .25		32' - .14		32' - .20		32' + .24		32' - .37		32' - .06	
36' - .22		36' + .02		36' - .10		36' - .00		36' - .58		36' - .29	
40' + 0.05		40' - 0.05		40' - 0.00		40' + 0.43		40' - 0.67		40' - 0.12	
44' - .02		44' + .45		44' + .22		44' + .28		44' - .68		44' - .20	
48' - .36		48' + .16		48' - .10		48' + .28		48' - .68		48' - .20	
52' - .24		52' - .17		52' - .20		52' + .15		52' - .92		52' - .38	
56' + .39		56' - .04		56' + .18		56' + .19		56' - .85		56' - .33	
10°-190°-0'	+ 0.17	100°-280°-0'	- 0.20	10°-100°-190°-280°-0'	- 0.01	14°-194°-0'	+ 0.07	104°-284°-0'	- 0.31	14°-104°-194°-284°-0'	- 0.12
4' + .32		4' - .56		4' - .12		4' - .38		4' - .52		4' - .45	
8' + .18		8' - .46		8' - .14		8' - .16		8' - .72		8' - .44	
12' - .40		12' - .31		12' - .36		12' - .54		12' - .54		12' - .54	
16' - .10		16' - .33		16' - .22		16' - .51		16' - .74		16' - .62	
20' + .02		20' - 0.30		20' - 0.14		20' - .54		20' - 0.37		20' - 0.46	
24' - .20		24' - .64		24' - .42		24' - .84		24' - .38		24' - .61	
28' + .06		28' - .10		28' - .02		28' - .70		28' - .50		28' - .60	
32' - .22		32' - .59		32' - .40		32' - 1.02		32' - .23		32' - .62	
36' + .07		36' - .40		36' - .16		36' - .89		36' - .28		36' - .58	
40' + 0.25		40' - .55		40' - .15		40' - 0.46		40' - 0.07		40' - 0.26	
44' - .10		44' - .82		44' - .46		44' - .68		44' - .12		44' - .40	
48' + .12		48' - 1.00		48' - .44		48' - .78		48' - .51		48' - .64	
52' + .23		52' - .84		52' - .30		52' - 1.13		52' - .18		52' - .66	
56' + .18		56' - .63		56' - .22		56' - .71		56' - .38		56' - .54	
11°-191°-0'	0.00	101°-281°-0'	- 0.24	11°-101°-191°-281°-0'	- 0.12	15°-195°-0'	- 0.23	105°-285°-0'	- 0.15	15°-105°-195°-285°-0'	- 0.19
4' - .28		4' - .06		4' - .17		4' - .80		4' - .23		4' - .52	
8' + .16		8' + .27		8' + .22		8' - .69		8' - .20		8' - .44	
12' - .10		12' + .20		12' + .05		12' - .59		12' - .39		12' - .49	
16' - .37		16' + .20		16' - .08		16' - .91		16' - .73		16' - .82	
20' - .25		20' - 0.20		20' - 0.22		20' - .91		20' - 0.53		20' - 0.72	
24' - .34		24' + .04		24' - .15		24' - .80		24' - .61		24' - .70	
28' - .30		28' + .16		28' - .07		28' - .58		28' - .24		28' - .41	
32' - .34		32' + .50		32' + .08		32' - .40		32' - .78		32' - .59	
36' + .10		36' + .48		36' + .29		36' - .14		36' - .70		36' - .42	
40' + 0.18		40' + 0.60		40' + 0.39		40' - 0.27		40' - 0.48		40' - 0.38	
44' - .11		44' + .29		44' + .09		44' - .60		44' - .66		44' - .63	
48' - .00		48' + .42		48' + .21		48' - .78		48' - .93		48' - .86	
52' - .02		52' + .38		52' + .18		52' - .62		52' - .38		52' - .50	
56' - .14		56' - .01		56' - .08		56' - .25		56' - .42		56' - .34	

OBSERVATORIO ASTRONÓMICO DE LA UNIVERSIDAD NACIONAL DE LA PLATA

Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4	Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4
16°-196°-0'	-0.42	106°-286°-0'	-0.09	16°-106°-196°-286°-0'	-0.25	20°-200°-0'	-0.05	110°-290°-0'	+0.19	20°-110°-200°-290°-0'	+0.07
4' - .06		4' - .04		4' - .25		4' - .26		4' + .36		4' + .05	
8' - .39		8' - .06		8' - .22		8' - .68		8' + .36		8' - .16	
12' - .47		12' - .34		12' - .40		12' - .18		12' + .09		12' - .04	
16' - .84		16' + .32		16' - .26		16' - .37		16' + .14		16' - .12	
20' - 0.61		20' - 0.18		20' - 0.40		20' - 0.14		20' + 0.03		20' - 0.06	
24' - .44		24' - .40		24' - .42		24' - 1.01		24' - .08		24' - .54	
28' - .36		28' - .42		28' - .39		28' - .82		28' - .17		28' - .50	
32' - .48		32' - .31		32' - .40		32' - .36		32' - .12		32' - .24	
36' - .76		36' + .04		36' - .36		36' - .71		36' - .40		36' - .56	
40' - 0.24		40' - 0.44		40' - 0.34		40' - 0.18		40' - 0.46		40' - 0.32	
44' + .17		44' - .12		44' + .02		44' - .32		44' - .48		44' - .40	
48' - .40		48' - .71		48' - .56		48' - .30		48' + .04		48' - .13	
52' - .10		52' - .14		52' - .12		52' - .20		52' - .06		52' - .13	
56' - .46		56' - .42		56' - .44		56' - .20		56' + .42		56' + .11	
17°-197°-0'	-0.15	107°-287°-0'	-0.13	17°-107°-197°-287°-0'	-0.14	21°-201°-0	0.13	111°-291°-0'	+0.38	21°-111°-201°-291°-0'	+0.13
4' - .07		4' + .14		4' + .04		4' - .32		4' + .22		4' - .05	
8' 00		8' + .20		8' + .10		8' - .26		8' + .32		8' + .03	
12' - .24		12' - .20		12' - .22		12' - .66		12' + .15		12' - .26	
16' - .14		16' - .02		16' - .08		16' - .44		16' + .12		16' - .16	
20' - 0.04		20' + 0.22		20' + 0.09		20' - 0.30		20' + 0.35		20' + 0.02	
24' - .38		24' 00		24' - .19		24' - .86		24' + .37		24' - .24	
28' - .14		28' + .27		28' + .06		28' - .82		28' + .72		28' - .05	
32' - .17		32' + .04		32' - .06		32' - .66		32' + .48		32' - .09	
36' - .36		36' + .06		36' - .15		36' - .24		36' + .26		36' + .01	
40' - 0.38		40' + 0.05		40' - 0.16		40' + 0.08		40' + .62		40' + 0.35	
44' - .21		44' + .11		44' - .05		44' + .02		44' + .52		44' + .27	
48' - .20		48' + .32		48' + .06		48' + .04		48' + .68		48' + .36	
52' + .18		52' + .39		52' + .28		52' - .05		52' + .64		52' + .30	
56' + .04		56' - .17		56' - .06		56' - .09		56' + .34		56' + .12	
18°-198°-0'	-0.02	108°-288°-0'	-0.12	18°-108°-198°-288°-0'	-0.07	22°-202°-0'	-0.16	112°-292°-0'	+0.06	22°-112°-202°-292°-0'	-0.05
4' - .50		4' - .48		4' - .49		4' - .33		4' - .17		4' - .25	
8' + .06		8' - .33		8' - .14		8' - .24		8' + .28		8' + .02	
12' + .04		12' - .20		12' - .08		12' - .68		12' - .10		12' - .39	
16' + .12		16' - .68		16' - .28		16' - .44		16' + .24		16' - .10	
20' + 0.05		20' - 0.08		20' - 0.02		20' - 0.19		20' - 0.09		20' - 0.14	
24' + .32		24' - .07		24' + .12		24' - .34		24' + .08		24' - .13	
28' + .31		28' - .40		28' - .04		28' + .16		28' + .08		28' + .12	
32' + .31		32' - .24		32' + .04		32' - .34		32' - .19		32' - .26	
36' + .32		36' - .07		36' + .12		36' - .46		36' + .06		36' - .20	
40' + 0.18		40' + 0.13		40' + 0.16		40' - 0.10		40' - 0.12		40' - 0.11	
44' + .59		44' + .42		44' + .50		44' - .25		44' - .19		44' - .22	
48' + .30		48' + .16		48' + .23		48' - .42		48' + .06		48' - .18	
52' + .13		52' + .12		52' + .12		52' - .16		52' - .14		52' - .15	
56' 00		56' - .38		56' - .19		56' - .37		56' + .16		56' - .10	
19°-199°-0'	-0.08	109°-289°-0'	-0.06	19°-109°-199°-289°-0'	-0.07	23°-203°-0'	+0.17	113°-293°-0'	+0.07	23°-113°-203°-293°-0'	+0.12
4' - .22		4' - .17		4' - .20		4' + .35		4' - .14		4' + .10	
8' - .55		8' - .41		8' - .48		8' + .48		8' - .16		8' + .16	
12' - .18		12' - .30		12' - .24		12' + .32		12' + .22		12' + .27	
16' 00		16' - .05		16' - .02		16' + .26		16' - .35		16' - .04	
20' - .11		20' - 0.16		20' - 0.14		20' + 0.16		20' - 0.17		20' 0.00	
24' + .24		24' - .12		24' + .06		24' + .12		24' - .22		24' - .05	
28' + .24		28' - .32		28' - .04		28' + .06		28' - .58		28' - .26	
32' + .17		32' + .01		32' + .09		32' - .06		32' - .49		32' - .28	
36' + .03		36' - .30		36' - .14		36' - .07		36' - .46		36' - .26	
40' + 0.18		40' + 0.10		40' + 0.14		40' - 0.14		40' + 0.04		40' - 0.05	
44' + .10		44' + .27		44' + .18		44' + .10		44' - .15		44' - .02	
48' + .01		48' - .08		48' - .04		48' + .32		48' + .06		48' + .19	
52' + .38		52' + .15		52' + .26		52' - .14		52' - .26		52' - .20	
56' - .06		56' + .03		56' - .02		56' - .18		56' - .30		56' - .24	

Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4	Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4
24°-204°-0'	-0.06	114°-294°-0'	-0.22	24°-114°-204°-294°-0'	-0.14	28°-208°-0'	-4.93	118°-298°-0'	+0.18	28°-118°-208°-298°-0'	-2.38
4'	.42	4'	.05	4'	.24	4'	-4.92	4'	.14	4'	-2.39
8'	.48	8'	.05	8'	.26	8'	-4.66	8'	.12	8'	-2.39
12'	.68	12'	.28	12'	.48	12'	-5.06	12'	.00	12'	-2.53
16'	.12	16'	.19	16'	.16	16'	-5.12	16'	.12	16'	-2.62
20'	-0.05	20'	-0.12	20'	-0.08	20'	-4.94	20'	-0.18	20'	-2.56
24'	+.51	24'	+.02	24'	+.26	24'	-5.66	24'	.21	24'	-2.94
28'	+.02	28'	-.43	28'	-.20	28'	-5.42	28'	.27	28'	-2.84
32'	+.10	32'	-.54	32'	-.22	32'	-5.50	32'	.32	32'	-2.91
36'	-.17	36'	-.10	36'	-.14	36'	-6.08	36'	+.22	36'	-2.93
40'	+.09	40'	-.44	40'	-.18	40'	-5.82	40'	+.13	40'	-2.84
44'	00	44'	-.11	44'	-.06	44'	-5.78	44'	+.39	44'	-2.70
48'	+.14	48'	-.34	48'	-.10	48'	-5.84	48'	-.04	48'	-.294
52'	+.06	52'	+.06	52'	+.06	52'	-5.82	52'	+.20	52'	-2.81
56'	+.24	56'	-.22	56'	+.01	56'	-5.40	56'	+.22	56'	-2.59
25°-205°-0'	-0.04	115°-295°-0'	+0.22	25°-115°-205°-295°-0'	+0.09	29°-209°-0'	-5.68	119°-299°-0'	+0.04	29°-119°-209°-299°-0'	-2.82
4'	+.02	4'	+.06	4'	+.04	4'	-5.74	4'	+.05	4'	-2.84
8'	.28	8'	.16	8'	.22	8'	-5.52	8'	.08	8'	-2.80
12'	.55	12'	.03	12'	.29	12'	-5.54	12'	.10	12'	-2.72
16'	.65	16'	.08	16'	.36	16'	-5.68	16'	.35	16'	-3.02
20'	-0.83	20'	0.00	20'	-0.42	20'	-5.03	20'	-0.46	20'	-2.74
24'	-.67	24'	-.08	24'	-.38	24'	-5.14	24'	.49	24'	-2.82
28'	-.52	28'	+.06	28'	-.23	28'	-4.98	28'	.80	28'	-2.89
32'	-.07	32'	+.24	32'	+.08	32'	-4.97	32'	.56	32'	-2.76
36'	-.32	36'	+.20	36'	-.06	36'	-4.84	36'	.29	36'	-2.56
40'	-.03	40'	+.42	40'	+.20	40'	-4.75	40'	-.52	40'	-2.61
44'	+.03	44'	+.26	44'	+.14	44'	-4.62	44'	-.14	44'	-2.38
48'	-.06	48'	+.60	48'	+.27	48'	-4.37	48'	.44	48'	-2.40
52'	-.02	52'	+.38	52'	+.18	52'	-4.04	52'	.31	52'	-2.18
56'	-.19	56'	+.31	56'	+.06	56'	-3.55	56'	.25	56'	-1.90
26°-206°-0'	+.02	116°-296°-0'	+0.10	26°-116°-206°-296°-0'	+0.06	30°-210°-0'	-3.30	120°-300°-0'	+0.08	30°-120°-210°-300°-0'	-1.61
4'	.40	4'	+.09	4'	.16	4'	-3.24	4'	.03	4'	-1.64
8'	.23	8'	.24	8'	.26	8'	-3.21	8'	.18	8'	-1.70
12'	+.12	12'	+.24	12'	+.18	12'	-2.98	12'	.50	12'	-1.74
16'	.42	16'	+.20	16'	.11	16'	-2.86	16'	.22	16'	-1.54
20'	+.10	20'	+.15	20'	+.12	20'	-2.70	20'	-.70	20'	-1.70
24'	+.04	24'	+.30	24'	+.17	24'	-2.14	24'	.69	24'	-1.42
28'	+.04	28'	+.26	28'	+.15	28'	-1.88	28'	.39	28'	-1.14
32'	+.27	32'	+.26	32'	+.26	32'	-1.58	32'	.13	32'	.86
36'	+.40	36'	+.36	36'	+.38	36'	-1.22	36'	.30	36'	.76
40'	+.20	40'	+.42	40'	+.31	40'	-0.87	40'	-.18	40'	-0.52
44'	-.26	44'	+.24	44'	-.01	44'	.68	44'	.14	44'	.41
48'	+.02	48'	+.02	48'	+.02	48'	.19	48'	.64	48'	.42
52'	-.54	52'	+.06	52'	-.24	52'	.43	52'	.53	52'	.48
56'	-.60	56'	+.09	56'	-.26	56'	.34	56'	.28	56'	.31
27°-207°-0'	-0.65	117°-297°-0'	+0.31	27°-117°-207°-297°-0'	-0.17	31°-211°-0'	+0.04	121°-301°-0'	+0.04	31°-121°-211°-301°-0'	+0.04
4'	.95	4'	+.16	4'	.40	4'	+.02	4'	.33	4'	.16
8'	-1.08	8'	+.06	8'	.51	8'	.00	8'	.54	8'	.27
12'	-1.64	12'	-.16	12'	-.90	12'	.42	12'	.62	12'	.52
16'	-1.80	16'	-.07	16'	.94	16'	-.56	16'	.66	16'	.61
20'	-2.01	20'	-.28	20'	-.14	20'	-0.47	20'	-0.51	20'	-0.49
24'	-2.28	24'	-.36	24'	-.32	24'	.50	24'	.36	24'	.43
28'	-2.61	28'	-.44	28'	-.52	28'	.42	28'	.32	28'	.37
32'	-2.72	32'	-.24	32'	-.24	32'	.05	32'	.30	32'	.18
36'	-3.75	36'	+.01	36'	-.87	36'	.64	36'	.50	36'	.57
40'	-3.60	40'	+.17	40'	-.72	40'	-0.30	40'	-0.03	40'	-0.16
44'	-4.10	44'	+.30	44'	-.90	44'	.36	44'	.19	44'	.28
48'	-4.04	48'	+.02	48'	-.01	48'	.26	48'	.28	48'	.27
52'	-4.24	52'	+.30	52'	-.97	52'	.28	52'	.36	52'	.32
56'	-4.61	56'	+.04	56'	-.28	56'	.26	56'	.50	56'	.38

Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4	Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4
32°-212°-0'	-0.15	122°-302°-0'	-0.15	32°-122°-212°-302°-0'	-0.15	36°-216°-0'	-0.86	126°-306°-0'	-0.30	36°-126°-216°-306°-0'	-0.58
4' - .21		4' - .38		4' - .30		4' - 1.10		4' - .26		4' - .68	
8' - .24		8' + .19		8' - .02		8' - .93		8' - .14		8' - .54	
12' - .61		12' - .16		12' - .38		12' - .33		12' - .27		12' - .30	
16' - .30		16' + .18		16' - .06		16' - .24		16' + .10		16' - .07	
20' - 0.58		20' + 0.08		20' - 0.25		20' - 0.22		20' - 0.15		20' - 0.18	
24' - .44		24' - .01		24' - .22		24' - .34		24' + .01		24' - .16	
28' - .56		28' + .12		28' - .22		28' - .20		28' + .06		28' - .07	
32' - .57		32' - .13		32' - .35		32' - .44		32' - .22		32' - .33	
36' - .44		36' - .30		36' - .37		36' - .73		36' - .61		36' - .64	
40' - 0.52		40' - 0.32		40' - 0.42		40' - 0.52		40' - 0.36		40' - 0.44	
44' - .52		44' - .40		44' - .46		44' - .84		44' - 0.00		44' - .42	
48' - .60		48' - .20		48' - .40		48' - .72		48' - .20		48' - .46	
52' - .58		52' - .08		52' - .33		52' - .94		52' - .16		52' - .55	
56' - .10		56' - .33		56' - .22		56' - .70		56' + .25		56' - .22	
33°-213°-0'	-0.37	123°-303°-0'	-0.31	33°-123°-213°-303°-0'	-0.34	37°-217°-0'	-0.27	127°-307°-0'	-0.05	37°-127°-217°-307°-0'	-0.16
4' - .44		4' - .48		4' - .46		4' - .14		4' + .09		4' - .02	
8' - .17		8' - .44		8' - .30		8' - .42		8' - .32		8' - .37	
12' - .32		12' - .54		12' - .43		12' - .42		12' - .20		12' - .31	
16' - .44		16' - .29		16' - .36		16' - .57		16' - .07		16' - .32	
20' - 0.16		20' - 0.68		20' - 0.42		20' - 0.70		20' + 0.02		20' - 0.34	
24' - .42		24' - .18		24' - .30		24' - .46		24' - .12		24' - .29	
28' - .98		28' - .60		28' - .79		28' - .46		26' - .29		28' - .38	
32' - .66		32' - .35		32' - .50		32' - .30		32' - .34		32' - .32	
36' - 1.02		36' - .24		36' - .63		36' - .64		36' + .11		36' - .26	
40' - 0.64		40' - 0.52		40' - 0.58		40' - 0.33		40' + 0.11		40' - 0.11	
44' - .52		44' - .51		44' - .52		44' - .54		44' + .13		44' - .20	
48' - .70		48' - .41		48' - .56		48' - .06		48' - .25		48' - .16	
52' - .83		52' - .48		52' - .66		52' - .26		52' - .42		52' - .34	
56' - .58		56' - .40		56' - .49		56' - .40		56' - .36		56' - .38	
34°-214°-0'	-0.27	124°-304°-0'	-0.06	34°-124°-214°-304°-0'	-0.17	38°-218°-0'	+ 0.14	128°-308°-0'	+ 0.04	38°-128°-218°-308°-0'	+ 0.09
4' - .28		4' - .92		4' - .60		4' + .02		4' - .10		4' - .04	
8' - .62		8' - .51		8' - .60		8' - .68		8' - .10		8' - .39	
12' - .88		12' - .61		12' - .74		12' - .10		12' + .19		12' + .04	
16' - .62		16' - .40		16' - .51		16' - .16		16' - .14		16' - .15	
20' - 1.43		20' - 0.40		20' - 0.92		20' + 0.14		20' - 0.18		20' - 0.02	
24' - .96		24' - .68		24' - .82		24' - .09		24' - 0.00		24' - .04	
28' - .98		28' - .68		28' - .83		28' - .02		28' + .36		28' + .17	
32' - 1.32		32' - .63		32' - .98		32' - .46		32' - .25		32' - .36	
36' - 1.20		36' - .65		36' - .92		36' - .04		36' - .22		36' - .13	
40' - 1.05		40' - 0.30		40' - 0.68		40' - 0.54		40' - 0.51		40' - 0.52	
44' - 1.29		44' - .90		44' - 1.10		44' - .50		44' - .25		44' - .38	
48' - 1.24		48' - .46		48' - .85		48' - .20		48' + .20		48' - .00	
52' - 1.29		52' - .28		52' - .78		52' - .32		52' - 0.00		52' - .16	
56' - 1.26		56' - .20		56' - .73		56' - .30		56' + .16		56' - .07	
35°-215°-0'	-1.03	125°-305°-0'	-0.43	35°-125°-215°-305°-0'	-0.73	39°-219°-0'	-0.18	129°-309°-0'	-0.02	39°-129°-219°-309°-0'	-0.10
4' - 1.34		4' - .04		4' - .69		4' - .03		4' - .16		4' - .10	
8' - 1.47		8' - .50		8' - .98		8' - .10		8' + .01		8' - .04	
12' - 1.52		12' - .92		12' - 1.22		12' + .02		12' - .04		12' - .01	
16' - 1.16		16' - .78		16' - .97		16' + .14		16' + .56		16' + .35	
20' - 1.32		20' - 0.86		20' - 1.09		20' - 0.23		20' + 0.14		20' - 0.04	
24' - 1.27		24' - .76		24' - 1.02		24' + .18		24' - .04		24' + .07	
28' - 1.34		28' - .88		28' - 1.11		28' - .12		28' - .20		28' - .16	
32' - 1.04		32' - 1.11		32' - 1.08		32' - .18		32' - .24		32' - .21	
36' - .83		36' - .64		36' - .74		36' - .04		36' - .34		36' - .19	
40' - 1.64		40' - 0.80		40' - 1.22		40' - 0.05		40' + 0.10		40' + 0.02	
44' - 1.54		44' - .56		44' - 1.05		44' + .18		44' + .10		44' + .14	
48' - 1.20		48' - .26		48' - .73		48' - .38		48' - .27		48' - .32	
52' - 1.54		52' - .27		52' - .90		52' - .18		52' - .21		52' - .20	
56' - 1.24		56' - .36		56' - .80		56' - .04		56' - .12		56' - .08	

Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4	Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4
$40^\circ-220^\circ-0'$	-0.52	$130^\circ-310^\circ-0'$	-0.37	$40^\circ-130^\circ-220^\circ-310^\circ-0'$	-0.44	$44^\circ-234^\circ-0'$	-0.31	$134^\circ-314^\circ-0'$	-0.05	$44^\circ-134^\circ-224^\circ-314^\circ-0'$	-0.18		
4'	.62	4'	+.12	4'	.25	4'	.04	4'	+.34	4'	+.15		
8'	.56	8'	.00	8'	.28	8'	.29	8'	.18	8'	.24		
12'	.28	12'	+.36	12'	+.04	12'	.25	12'	.37	12'	.31		
16'	.16	16'	-.14	16'	-.15	16'	-.04	16'	-.35	16'	-.20		
20'	-0.17	20'	-0.04	20'	-0.10	20'	-.09	20'	-.10	20'	-.10		
24'	-.06	24'	-.16	24'	-.11	24'	-.02	24'	-.44	24'	-.23		
28'	-.07	28'	+.22	28'	+.08	28'	-.01	28'	-.24	28'	-.12		
32'	-.20	32'	+.12	32'	-.04	32'	.32	32'	-.20	32'	-.26		
36'	-.18	36'	-.07	36'	-.12	36'	+.24	36'	-.14	36'	+.05		
40'	-0.26	40'	-0.41	40'	-0.34	40'	.36	40'	-.42	40'	-.39		
44'	.28	44'	-.16	44'	.22	44'	.46	44'	.17	44'	.32		
48'	.10	48'	+.49	48'	+.15	48'	.11	48'	.28	48'	.20		
52'	.65	52'	+.10	52'	.28	52'	.55	52'	.42	52'	.48		
56'	+.02	56'	-.18	56'	-.08	56'	.41	56'	.33	56'	.37		
$41^\circ-221^\circ-0'$	-0.19	$131^\circ-311^\circ-0'$	+.15	$41^\circ-131^\circ-221^\circ-311^\circ-0'$	-0.02	$45^\circ-235^\circ-0'$	-.33	$135^\circ-315^\circ-0'$	+.08	$45^\circ-135^\circ-225^\circ-315^\circ-0'$	-.12		
4'	.29	4'	-.09	4'	-.19	4'	.28	4'	-.14	4'	-.21		
8'	-.04	8'	+.14	8'	+.05	8'	-.06	8'	+.35	8'	+.20		
12'	.32	12'	-.10	12'	-.21	12'	-.04	12'	-.10	12'	-.07		
16'	.16	16'	-.16	16'	-.16	16'	+.30	16'	+.22	16'	+.26		
20'	-0.37	20'	+.13	20'	-0.12	20'	+.72	20'	+.14	20'	+.43		
24'	.46	24'	-.12	24'	-.29	24'	.36	24'	-.05	24'	+.16		
28'	.61	28'	+.07	28'	-.27	28'	.30	28'	-.02	28'	+.14		
32'	.37	32'	-.12	32'	-.24	32'	+.10	32'	+.05	32'	+.08		
36'	.50	36'	+.06	36'	-.22	36'	+.20	36'	-.10	36'	+.05		
40'	-0.76	40'	-0.08	40'	-0.42	40'	+.30	40'	-.05	40'	+.12		
44'	.34	44'	+.07	44'	-.14	44'	-.14	44'	-.16	44'	-.15		
48'	.67	48'	-.13	48'	-.40	48'	+.08	48'	+.02	48'	+.05		
52'	.10	52'	-.17	52'	-.14	52'	-.08	52'	-.26	52'	-.17		
56'	.64	56'	-.14	56'	-.39	56'	-.20	56'	-.19	56'	-.20		
$42^\circ-222^\circ-0'$	-0.24	$132^\circ-312^\circ-0'$	+.12	$42^\circ-132^\circ-222^\circ-312^\circ-0'$	-0.06	$46^\circ-226^\circ-0'$	-.23	$136^\circ-316^\circ-0'$	+.09	$46^\circ-136^\circ-226^\circ-316^\circ-0'$	-.07		
4'	.68	4'	-.30	4'	-.49	4'	-.02	4'	-.01	4'	-.02		
8'	.72	8'	-.38	8'	-.55	8'	.52	8'	+.05	8'	-.24		
12'	.64	12'	+.02	12'	-.31	12'	.38	12'	+.36	12'	-.01		
16'	.76	16'	-.66	16'	.71	16'	-.12	16'	+.40	16'	+.14		
20'	-0.80	20'	-.37	20'	-.58	20'	+.36	20'	+.34	20'	+.35		
24'	.68	24'	-.19	24'	-.44	24'	+.34	24'	+.22	24'	+.28		
28'	.95	28'	-.42	28'	-.68	28'	-.27	28'	-.12	28'	-.20		
32'	.78	32'	-.30	32'	-.54	32'	-.24	32'	+.06	32'	-.09		
36'	-1.04	36'	-.07	36'	-.56	36'	-.52	36'	-.06	36'	-.29		
40'	-0.76	40'	-.34	40'	-.55	40'	-.10	40'	-.13	40'	-.12		
44'	.95	44'	-.24	44'	-.60	44'	.14	44'	-.02	44'	-.08		
48'	.88	48'	-.16	48'	-.52	48'	.24	48'	+.12	48'	-.06		
52'	.90	52'	-.32	52'	-.61	52'	.14	52'	-.28	52'	-.21		
56'	.90	56'	-.08	56'	-.49	56'	.38	56'	-.03	56'	-.20		
$43^\circ-223^\circ-0'$	-0.45	$133^\circ-313^\circ-0'$	+.09	$43^\circ-133^\circ-223^\circ-313^\circ-0'$	-0.18	$47^\circ-227^\circ-0'$	-.19	$137^\circ-317^\circ-0'$	+.24	$47^\circ-137^\circ-227^\circ-317^\circ-0'$	+.03		
4'	.64	4'	+.20	4'	-.22	4'	.38	4'	-.38	4'	-.38		
8'	.56	8'	-.45	8'	-.50	8'	.16	8'	+.13	8'	-.02		
12'	.61	12'	-.28	12'	-.44	12'	.24	12'	+.17	12'	-.04		
16'	.78	16'	-.33	16'	-.56	16'	.24	16'	-.15	16'	-.20		
20'	-0.60	20'	-.12	20'	-.36	20'	.10	20'	+.28	20'	+.09		
24'	.77	24'	-.38	24'	-.58	24'	.08	24'	+.14	24'	+.03		
28'	.86	28'	-.15	28'	-.50	28'	.44	28'	+.60	28'	+.08		
32'	.52	32'	-.02	32'	-.27	32'	.28	32'	+.42	32'	+.07		
36'	.40	36'	-.12	36'	-.26	36'	.58	36'	+.32	36'	-.13		
40'	.54	40'	.31	40'	.42	40'	.50	40'	.23	40'	.14		
44'	.13	44'	.31	44'	.22	44'	.46	44'	.23	44'	.12		
48'	.50	48'	.14	48'	.32	48'	.66	48'	.42	48'	.12		
52'	.28	52'	.08	52'	.18	52'	.40	52'	.22	52'	.09		
56'	.41	56'	-.09	56'	-.25	56'	-.23	56'	-.10	56'	-.06		

OBSERVATORIO ASTRONÓMICO DE LA UNIVERSIDAD NACIONAL DE LA PLATA

Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4	Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4
$48^\circ-228^\circ-0'$	— .02	$138^\circ-318^\circ-0'$	+ .17	$48^\circ-138^\circ-228^\circ-318^\circ-0'$	+ .07	$52^\circ-232^\circ-0'$	— .17	$142^\circ-322^\circ-0'$	+ .36	$52^\circ-142^\circ-232^\circ-322^\circ-0'$	+ .09
4' — .34	4' + .46	4' — .10	4' + .06	4' — .17	4' + .22	4' — .22	4' + .71	4' — .17	4' + .22	4' — .02	8' + .34
8' — .28	8' + .10	8' — .09	8' — .04	8' — .44	8' + .02	8' — .21	8' + .29	8' — .21	8' + .29	12' — .21	16' + .16
12' — .16	12' + .55	12' + .20	12' + .03	12' + .29	12' + .29	12' + .02	12' + .29	12' + .29	12' + .29	16' + .16	20' — .23
16' + .08	16' + .46	16' + .27	16' + .03	16' + .27	16' + .27	16' + .29	16' + .29	16' + .29	16' + .29	20' — .23	24' — .34
20' — .34	20' + .40	20' + .03	20' — .42	20' — .42	20' — .42	20' — .04	20' — .04	20' — .04	20' — .04	24' — .34	28' — .12
24' — .32	24' + .22	24' — .05	24' — .24	24' — .24	24' — .24	24' — .44	24' — .44	24' — .44	24' — .44	28' — .12	32' + .01
28' — .33	28' + .52	28' + .10	28' — .21	28' — .21	28' — .21	28' — .04	28' — .04	28' — .04	28' — .04	32' + .01	36' + .04
32' — .42	32' + .80	32' + .19	32' — .10	32' — .10	32' — .10	32' + .12	32' + .12	32' + .12	32' + .12	36' + .04	40' + .24
36' — .39	36' + .22	36' — .08	36' + .03	36' + .03	36' + .03	36' + .06	36' + .06	36' + .06	36' + .06	40' + .24	44' + .04
40' — .39	40' + .36	40' — .02	40' + .32	40' + .32	40' + .32	40' + .16	40' + .16	40' + .16	40' + .16	44' + .04	48' + .02
44' — .66	44' + .92	44' + .13	44' — .02	44' + .11	44' + .11	44' + .06	44' + .06	44' + .06	44' + .06	48' + .02	52' + .02
48' — .50	48' + .05	48' — .22	48' + .09	48' + .09	48' + .09	48' — .06	48' — .06	48' — .06	48' — .06	52' + .02	56' — .12
52' — .26	52' + .52	52' + .13	52' + .07	52' + .07	52' + .07	52' — .02	52' — .02	52' — .02	52' — .02	56' — .12	20' — .20
56' — .54	56' + .29	56' — .12	56' — .24	56' — .24	56' — .24	56' — .00	56' — .00	56' — .00	56' — .00	20' — .20	24' — .46
$49^\circ-229^\circ-0'$	+ .06	$139^\circ-319^\circ-0'$	+ .15	$49^\circ-139^\circ-229^\circ-319^\circ-0'$	+ .11	$53^\circ-233^\circ-0'$	— .15	$143^\circ-323^\circ-0'$	+ .06	$53^\circ-143^\circ-233^\circ-323^\circ-0'$	— .05
4' .00	4' + .14	4' + .07	4' — .32	4' + .04	4' + .04	4' — .14	4' — .14	4' — .14	4' — .14	8' — .40	12' — .20
8' — .30	8' — .55	8' — .42	8' — .59	8' — .20	8' — .20	8' — .20	8' — .20	8' — .20	8' — .20	12' — .20	16' — .36
12' — .08	12' — .41	12' — .24	12' — .49	12' + .09	12' + .09	12' + .09	12' + .09	12' + .09	12' + .09	16' — .36	20' — .20
16' + .14	16' — .52	16' — .19	16' — .68	16' — .05	16' — .05	16' — .05	16' — .05	16' — .05	16' — .05	20' — .20	24' — .46
20' + .08	20' — .24	20' — .08	20' — .50	20' + .09	20' + .09	20' + .09	20' + .09	20' + .09	20' + .09	24' — .46	28' — .12
24' + .40	24' — .14	24' + .13	24' — 1.02	24' + .11	24' + .11	24' + .11	24' + .11	24' + .11	24' + .11	28' — .12	32' — .40
28' — .16	28' — .11	28' — .14	28' — .32	28' + .09	28' + .09	28' + .09	28' + .09	28' + .09	28' + .09	32' — .40	36' — .18
32' + .12	32' + .08	32' + .10	32' — .54	32' — .25	32' — .25	32' — .25	32' — .25	32' — .25	32' — .25	36' — .18	40' — .32
36' — .16	36' — .02	36' — .09	36' — .04	36' — .32	36' — .32	36' — .32	36' — .32	36' — .32	36' — .32	40' — .32	44' — .64
40' — .01	40' — .25	40' — .13	40' — .67	40' + .04	40' + .04	40' + .04	40' + .04	40' + .04	40' + .04	44' — .64	48' — .17
44' — .26	44' + .05	44' — .10	44' — .94	44' — .33	44' — .33	44' — .33	44' — .33	44' — .33	44' — .33	48' — .17	52' — .30
48' + .33	48' — .30	48' — .03	48' — .47	48' + .13	48' + .13	48' + .13	48' + .13	48' + .13	48' + .13	52' — .30	56' — .30
52' + .08	52' — .20	52' — .06	52' — .38	52' — .23	52' — .23	52' — .23	52' — .23	52' — .23	52' — .23	56' — .30	20' — .12
56' + .24	56' — .06	56' + .09	56' — .45	56' — .16	56' — .16	56' — .16	56' — .16	56' — .16	56' — .16	20' — .12	24' — .13
$50^\circ-230^\circ-0'$	+ 0.05	$140^\circ-320^\circ-0'$	+ 0.27	$50^\circ-140^\circ-230^\circ-320^\circ-0'$	+ 0.16	$54^\circ-234^\circ-0'$	— .14	$144^\circ-324^\circ-0'$	+ .12	$54^\circ-144^\circ-234^\circ-324^\circ-0'$	— .01
4' + .36	4' — .06	4' + .15	4' — .21	4' — .12	4' — .12	4' — .12	4' — .12	4' — .12	4' — .12	8' — .26	12' — .31
8' + .18	8' + .04	8' + .11	8' — .17	8' — .36	8' — .36	8' — .36	8' — .36	8' — .36	8' — .36	12' — .31	16' — .09
12' + .02	12' + .06	12' + .04	12' — .24	12' — .38	12' — .38	12' — .38	12' — .38	12' — .38	12' — .38	16' — .09	20' — .12
16' — .05	16' + .14	16' + .04	16' + .25	16' + .43	16' + .43	16' + .43	16' + .43	16' + .43	16' + .43	20' — .12	24' — .13
20' + .32	20' + .21	20' + .26	20' — .21	20' — .02	20' — .02	20' — .02	20' — .02	20' — .02	20' — .02	24' — .13	28' — .11
24' + .64	24' + .04	24' + .34	24' — .02	24' — .24	24' — .24	24' — .24	24' — .24	24' — .24	24' — .24	28' — .11	32' — .04
28' + .35	28' + .16	28' + .26	28' — .26	28' + .04	28' + .04	28' + .04	28' + .04	28' + .04	28' + .04	32' — .04	36' — .15
32' + .12	32' + .42	32' + .27	32' — .14	32' + .06	32' + .06	32' + .06	32' + .06	32' + .06	32' + .06	36' — .15	40' — .02
36' — .18	36' + .40	36' + .11	36' — .04	36' — .26	36' — .26	36' — .26	36' — .26	36' — .26	36' — .26	40' — .02	44' + .18
40' — .12	40' + .56	40' + .22	40' — .26	40' + .22	40' + .22	40' + .22	40' + .22	40' + .22	40' + .22	44' + .18	48' + .16
44' .00	44' + .22	44' + .11	44' + .16	44' + .20	44' + .20	44' + .20	44' + .20	44' + .20	44' + .20	48' + .16	52' + .40
48' + .39	48' + .42	48' + .40	48' — .02	48' + .35	48' + .35	48' + .35	48' + .35	48' + .35	48' + .35	52' + .40	56' + .16
52' + .34	52' + .62	52' + .48	52' + .28	52' + .51	52' + .51	52' + .51	52' + .51	52' + .51	52' + .51	56' + .16	20' — .18
56' + .14	56' + .25	56' + .20	56' + .11	56' + .20	56' + .20	56' + .20	56' + .20	56' + .20	56' + .20	20' — .18	24' — .10
$51^\circ-231^\circ-0'$	— .10	$141^\circ-321^\circ-0'$	+ .10	$51^\circ-141^\circ-231^\circ-321^\circ-0'$.00	$55^\circ-235^\circ-0'$	+ .12	$145^\circ-325^\circ-0'$	+ .17	$55^\circ-145^\circ-235^\circ-325^\circ-0'$	+ .14
4' — .02	4' — .02	4' — .02	4' + .11	4' + .34	4' + .34	4' + .34	4' + .34	4' + .34	4' + .34	8' — .11	12' — .17
8' + .06	8' + .14	8' + .10	8' — .24	8' + .02	8' + .02	8' + .02	8' + .02	8' + .02	8' + .02	12' — .17	16' + .37
12' — .02	12' + .56	12' + .27	12' — .44	12' + .10	12' + .10	12' + .10	12' + .10	12' + .10	12' + .10	16' + .37	20' — .18
16' — .18	16' + .41	16' + .12	16' — .16	16' + .90	16' + .90	16' + .90	16' + .90	16' + .90	16' + .90	20' — .18	24' — .02
20' — .06	20' + .52	20' + .23	20' — .10	20' + .46	20' + .46	20' + .46	20' + .46	20' + .46	20' + .46	24' — .02	28' — .18
24' + .24	24' + .54	24' + .39	24' — .40	24' + .20	24' + .20	24' + .20	24' + .20	24' + .20	24' + .20	28' — .18	32' — .18
28' + .20	28' + .38	28' + .29	28' — .54	28' + .50	28' + .50	28' + .50	28' + .50	28' + .50	28' + .50	32' — .18	36' — .40
32' + .15	32' + .56	32' + .36	32' — .60	32' + .23	32' + .23	32' + .23	32' + .23	32' + .23	32' + .23	36' — .40	40' — .18
36' + .19	36' + .50	36' + .34	36' — .62	36' + .19	36' + .19	36' + .19	36' + .19	36' + .19	36' + .19	40' — .18	44' — .09
40' + .56	40' + .56	40' + .56	40' — .45	40' + .09	40' + .09	40' + .09	40' + .09	40' + .09	40' + .09	44' — .09	48' — .18
44' + .24	44' + .41	44' + .32	44' — .30	44' + .12	44' + .12	44' + .12	44' + .12	44' + .12	44' + .12	48' — .18	52' — .09
48' — .16	48' + .51	48' + .18	48' — .39	48' + .04	48' + .04	48' + .04	48' + .04	48' + .04	48' + .04	52' — .09	56' — .12
52' — .09	52' + .7										

Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4	Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4
56°-236°-0'	+ .16	146°-326°-0'	+ .08	56°-146°-236°-326°-0'	+ .12	60°-240°-0'	+ 0.27	150°-330°-0'	+ 0.21	60°-150°-240°-330°-0'	+ 0.24
4' + .27		4' — .28		4' + .00		4' — .10		4' — .28		4' — .19	
8' + .42		8' + .08		8' + .25		8' + .20		8' — .48		8' — .14	
12' + .69		12' — .26		12' + .22		12' — .10		12' — .26		12' — .18	
16' + .95		16' + .24		16' + .60		16' — .27		16' — .46		16' — .36	
20' + .66		20' + .41		20' + .54		20' — 0.32		20' — 0.11		20' — 0.22	
24' + .84		24' + .34		24' + .59		24' + .06		24' — .16		24' — .05	
28' + .33		28' + .37		28' + .35		28' 00		28' — .30		28' — .15	
32' + .36		32' + .12		32' + .24		32' + .19		32' — .24		32' — .02	
36' + .09		36' + .52		36' + .30		36' + .18		36' + .03		36' + .10	
40' + .62		40' + .22		40' + .12		40' + 0.43		40' + 0.11		40' + 0.27	
44' + .29		44' + .18		44' + .24		44' + .16		44' + .01		44' + .08	
48' + .72		48' + .20		48' + .46		48' + .18		48' + .28		48' + .23	
52' + .40		52' — .08		52' + .16		52' — .06		52' + .26		52' + .10	
56' + .66		56' — .07		56' + .30		56' + .13		56' — .09		56' + .02	
57°-237°-0'	+ .40	147°-327°-0'	+ .38	57°-147°-237°-327°-0'	+ .39	61°-241°-0'	+ 0.12	151°-331°-0'	+ 0.20	61°-151°-241°-331°-0'	+ 0.16
4' + .58		4' + .68		4' + .63		4' + .14		4' — .04		4' + .05	
8' + .36		8' + .91		8' + .64		8' + .06		8' + .21		8' + .14	
12' + .46		12' + .84		12' + .65		12' + .22		12' — .14		12' + .04	
16' + .61		16' + .51		16' + .56		16' + .26		16' + .20		16' + .23	
20' + .46		20' + .19		20' + .32		20' + 0.06		20' + 0.18		20' + 0.12	
24' + .54		24' + .22		24' + .38		24' + .08		24' — .28		24' — .10	
28' + .60		28' + .20		28' + .40		28' + .18		28' — .04		28' + .07	
32' + .38		32' — .02		32' + .18		32' + .18		32' — .31		32' — .06	
36' + .78		36' + .04		36' + .41		36' — .38		36' — .10		36' — .24	
40' + .74		40' + .09		40' + .42		40' + 0.04		40' + 0.08		40' + 0.06	
44' + .49		44' — .16		44' + .16		44' + .12		44' + .02		44' + .07	
48' + .30		48' + .02		48' + .16		48' + .18		48' + .22		48' + .20	
52' + .41		52' + .05		52' + .23		52' — .22		52' + .22		52' 00	
56' + .32		56' + .12		56' + .22		56' — .18		56' — .16		56' — .17	
58°-238°-0'	+ .59	148°-328°-0'	+ .34	58°-148°-238°-328°-0'	+ .46	62°-242°-0'	— 0.09	152°-332°-0'	— 0.12	62°-152°-242°-332°-0'	— 0.11
4' + .24		4' + .21		4' + .22		4' + .56		4' — .43		4' + .06	
8' + .16		8' + .49		8' + .32		8' + .05		8' — .27		8' — .11	
12' + .08		12' + .21		12' + .15		12' + .28		12' + .02		12' + .15	
16' + .25		16' + .18		16' + .22		16' — .18		16' — .20		16' — .19	
20' + .31		20' + .58		20' + .44		20' + 0.24		20' — 0.21		20' + 0.02	
24' + .42		24' + .34		24' + .38		24' 00		24' + .02		24' + .01	
28' + .74		28' + .29		28' + .52		28' — .09		28' — .18		28' — .14	
32' + .59		32' + .36		32' + .48		32' — .04		32' + .23		32' + .10	
36' + .54		36' + .38		36' + .46		36' — .04		36' + .06		36' + .01	
40' + .37		40' + .70		40' + .54		40' — 0.14		40' + 0.07		40' — 0.04	
44' + .58		44' + .36		44' + .47		44' + .24		44' + .18		44' + .21	
48' + .37		48' + .70		48' + .54		48' + .06		48' — .15		48' — .04	
52' + .66		52' + .70		52' + .68		52' — .08		52' — .05		52' — .06	
56' + .78		56' + .76		56' + .77		56' — .08		56' — .14		56' — .11	
59°-239°-0'	+ .10	149°-329°-0'	+ .84	59°-149°-239°-329°-0'	+ .47	63°-243°-0'	+ 0.16	153°-333°-0'	+ 0.14	63°-153°-243°-333°-0'	+ 0.15
4' + .51		4' + .60		4' + .56		4' + .34		4' + .07		4' + .20	
8' + .18		8' + .26		8' + .22		8' + .30		8' + .46		8' + .38	
12' + .04		12' + .10		12' + .07		12' + .20		12' — .08		12' + .06	
16' + .15		16' + .35		16' + .25		16' + .14		16' — .18		16' — .02	
20' + .40		20' — .08		20' + .16		20' + 0.18		20' + 0.33		20' + 0.26	
24' + .35		24' — .04		24' + .16		24' + .30		24' + .58		24' + .44	
28' + .38		28' — .14		28' + .12		28' + .58		28' + .37		28' + .48	
32' + .63		32' — .10		32' + .26		32' + .44		32' + .46		32' + .45	
36' + .26		36' + .07		36' + .16		36' + .26		36' + .68		36' + .47	
40' + .40		40' — .06		40' + .17		40' + 0.24		40' + 0.94		40' + 0.59	
44' + .47		44' + .05		44' + .26		44' + .21		44' + .92		44' + .56	
48' + .20		48' — .22		48' — .01		48' — .02		48' + .86		48' + .42	
52' + .45		52' — .22		52' + .12		52' — .25		52' + .48		52' + .12	
56' — .10		56' — .34		56' — .22		56' — .04		56' + .86		56' + .41	

OBSERVATORIO ASTRONÓMICO DE LA UNIVERSIDAD NACIONAL DE LA PLATA

Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4	Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4
$64^\circ-244^\circ-0'$	+ 0.06	$154^\circ-334^\circ-0'$	+ 0.13	$64^\circ-154^\circ-244^\circ-334^\circ-0'$	+ 0.10	$68^\circ-248^\circ-0'$	+ 0.09	$158^\circ-338^\circ-0'$	- 0.28	$68^\circ-158^\circ-248^\circ-338^\circ-0'$	- 0.09
4'— .12		4'— .90		4'— .39		4'— .33		4'— .80		4'— .24	
8'— .32		8'— .66		8'— .17		8'— .27		8'— .48		8'— .10	
12'— .34		12'— .88		12'— .27		12'— .37		12'— .82		12'— .22	
16'— .52		16'— .74		16'— .11		16'— .42		16'— .86		16'— .22	
20'— 0.69		20'— 0.88		20'— 0.10		20'— 0.38		20'— 0.78		20'— 0.20	
24'— .44		24'— .86		24'— .21		24'— .33		24'— 1.00		24'— .34	
28'— .07		28'— .38		28'— .16		28'— .38		28'— .96		28'— .29	
32'— + .06		32'— + .18		32'— + .12		32'— + .32		32'— 1.42		32'— .55	
36'— .18		36'— + .74		36'— + .28		36'— + .10		36'— .61		36'— .26	
40'— 0.19		40'— 0.43		40'— 0.12		40'— 0.20		40'— 0.44		40'— 0.12	
44'— .45		44'— .58		44'— 6		44'— .02		44'— .70		44'— .34	
48'— .18		48'— .42		48'— .12		48'— .04		48'— .36		48'— .20	
52'— .15		52'— + .23		52'— 4		52'— + .12		52'— .39		52'— .14	
56'— .32		56'— .24		56'— .28		56'— .12		56'— .27		56'— .20	
$65^\circ-245^\circ-0'$	- 0.15	$155^\circ-335^\circ-0'$	+ 0.46	$65^\circ-155^\circ-245^\circ-335^\circ-0'$	+ 0.15	$69^\circ-249^\circ-0'$	0.00	$159^\circ-339^\circ-0'$	- 0.07	$69^\circ-159^\circ-249^\circ-339^\circ-0'$	- 0.03
4'— .21		4'— .04		4'— .12		4'— .12		4'— .04		4'— .08	
8'— .43		8'— + .16		8'— .14		8'— .01		8'— .36		8'— .18	
12'— .55		12'— + .04		12'— .25		12'— .08		12'— .33		12'— .20	
16'— .62		16'— .40		16'— .51		16'— + .03		16'— .48		16'— .22	
20'— 0.44		20'— 0.08		20'— 0.26		20'— 0.22		20'— 0.00		20'— 0.11	
24'— .78		24'— .12		24'— .45		24'— + .08		24'— .43		24'— .18	
28'— .26		28'— .34		28'— .30		28'— .01		28'— .08		28'— .04	
32'— .32		32'— .22		32'— .27		32'— .33		32'— + .23		32'— .05	
36'— .08		36'— .11		36'— .10		36'— .24		36'— .23		36'— .24	
40'— 0.17		40'— 0.08		40'— 0.12		40'— 0.09		40'— 0.06		40'— 0.02	
44'— .03		44'— .36		44'— .20		44'— + .11		44'— .12		44'— 00	
48'— .14		48'— .44		48'— .29		48'— + .10		48'— .19		48'— .04	
52'— .13		52'— + .52		52'— + .20		52'— .14		52'— .28		52'— .21	
56'— .06		56'— .20		56'— .13		56'— .36		56'— .38		56'— .37	
$66^\circ-246^\circ-0'$	+ 0.02	$156^\circ-336^\circ-0'$	0.00	$66^\circ-156^\circ-246^\circ-336^\circ-0'$	+ 0.01	$70^\circ-250^\circ-0'$	- 0.10	$160^\circ-340^\circ-0'$	- 0.26	$70^\circ-160^\circ-250^\circ-340^\circ-0'$	- 0.18
4'— .04		4'— .02		4'— .01		4'— .27		4'— .66		4'— .46	
8'— .05		8'— + .09		8'— .02		8'— + .36		8'— .21		8'— + .08	
12'— .26		12'— + .10		12'— .08		12'— .12		12'— .40		12'— .26	
16'— + .04		16'— + .20		16'— + .12		16'— + .62		16'— .46		16'— + .08	
20'— 0.24		20'— + .70		20'— + .23		20'— + .56		20'— 0.14		20'— + .21	
24'— .22		24'— + .21		24'— 00		24'— .15		24'— .23		24'— .19	
28'— .52		28'— + .16		28'— .18		28'— .12		28'— .38		28'— .25	
32'— + .08		32'— .06		32'— + .01		32'— + .15		32'— .24		32'— .04	
36'— .08		36'— + .17		36'— + .04		36'— + .08		36'— .07		36'— 00	
40'— 0.32		40'— + .44		40'— + 0.06		40'— + .62		40'— + 0.24		40'— + 0.43	
44'— .48		44'— + .31		44'— .08		44'— + .32		44'— .20		44'— + .06	
48'— .04		48'— + .42		48'— + .19		48'— .12		48'— .26		48'— .19	
52'— + .04		52'— + .18		52'— + .11		52'— .28		52'— .03		52'— .16	
56'— .02		56'— + .18		56'— + .08		56'— .10		56'— .19		56'— .14	
$67^\circ-247^\circ-0'$	+ 0.26	$157^\circ-337^\circ-0'$	- 0.10	$67^\circ-157^\circ-247^\circ-337^\circ-0'$	+ 0.08	$71^\circ-251^\circ-0'$	+ 0.06	$161^\circ-341^\circ-0'$	- 0.14	$71^\circ-161^\circ-251^\circ-341^\circ-0'$	- 0.04
4'— + .10		4'— .22		4'— .06		4'— + .06		4'— .05		4'— 00	
8'— + .28		8'— .17		8'— + .06		8'— .20		8'— .40		8'— .30	
12'— + .15		12'— .10		12'— + .02		12'— .47		12'— .02		12'— .24	
16'— + .11		16'— .12		16'— 00		16'— .33		16'— .30		16'— .32	
20'— + .10		20'— 0.16		20'— 0.03		20'— 0.46		20'— 0.06		20'— 0.20	
24'— + .27		24'— .37		24'— .05		24'— .82		24'— .30		24'— .31	
28'— + .23		28'— .02		28'— + .10		28'— .48		28'— .32		28'— .40	
32'— + .36		32'— .28		32'— + .04		32'— .64		32'— .51		32'— .58	
36'— + .38		36'— .14		36'— + .12		36'— .61		36'— .28		36'— .44	
40'— + 0.44		40'— 0.17		40'— + 0.14		40'— 0.52		40'— 0.42		40'— 0.47	
44'— + .48		44'— .36		44'— + .06		44'— .10		44'— .58		44'— .34	
48'— + .25		48'— + .02		48'— + .14		48'— .20		48'— .27		48'— .24	
52'— + .04		52'— .16		52'— .06		52'— .03		52'— .24		52'— .14	
56'— + .14		56'— .15		56'— 00		56'— .30		56'— .27		56'— .28	

Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4	Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4
72°-252°-0'	- 0.10	162°-342°-0'	- 0.30	72°-162°-252°-342°-0'	- 0.20	76°-256°-0'	+ 0.30	166°-346°-0'	+ 0.22	76°-166°-256°-346°-0'	+ 0.26
4'	- .60	4'	- .27	4'	- .44	4'	.00	4'	- .45	4'	+ .22
8'	- .42	8'	- .15	8'	- .38	8'	+ .08	8'	- .60	8'	+ .34
12'	- .37	12'	- .08	12'	- .22	12'	+ .12	12'	- .49	12'	+ .30
16'	- .31	16'	- .64	16'	- .48	16'	+ .02	16'	- .54	16'	+ .28
20'	- 0.57	20'	- 0.64	20'	- 0.60	20'	+ 0.36	20'	+ 0.57	20'	+ 0.46
24'	- .49	24'	- .36	24'	- .42	24'	+ .08	24'	- .56	24'	+ .32
28'	- .48	28'	- .42	28'	- .45	28'	- .19	28'	- .52	28'	+ .16
32'	- .46	32'	- 1.00	32'	- .73	32'	- .09	32'	- .56	32'	+ .24
36'	- .38	36'	- .60	36'	- .49	36'	- .06	36'	- .59	36'	+ .26
40'	- 0.44	40'	- 0.48	40'	- 0.46	40'	+ 0.18	40'	- 0.35	40'	+ 0.26
44'	+ .07	44'	- .50	44'	- .22	44'	+ .34	44'	- .19	44'	+ .08
48'	- .17	48'	- .23	48'	- .20	48'	+ .16	48'	- .21	48'	+ .18
52'	- .12	52'	+ .06	52'	- .03	52'	+ .46	52'	- .08	52'	+ .19
56'	- .20	56'	- .28	56'	- .24	56'	+ .08	56'	- .19	56'	+ .14
73°-253°-0'	+ 0.02	163°-343°-0'	+ 0.03	73°-163°-253°-343°-0'	+ 0.02	77°-257°-0'	+ 0.41	167°-347°-0'	+ 0.28	77°-167°-257°-347°-0'	+ 0.34
4'	+ .07	4'	+ .58	4'	+ .32	4'	+ .76	4'	+ .36	4'	+ .56
8'	- .14	8'	+ .42	8'	+ .14	8'	+ .66	8'	+ .44	8'	+ .55
12'	- .21	12'	+ .46	12'	+ .12	12'	+ .55	12'	+ .30	12'	+ .42
16'	- .70	16'	+ .48	16'	- .11	16'	+ .34	16'	- .10	16'	+ .12
20'	- 0.27	20'	+ 0.50	20'	+ 0.12	20'	+ 0.54	20'	+ 0.48	20'	+ 0.51
24'	- .71	24'	+ .50	24'	- .10	24'	+ .68	24'	- .13	24'	+ .28
28'	- .78	28'	+ .49	28'	- .14	28'	+ 1.12	28'	+ .26	28'	+ .69
32'	- .34	32'	+ .61	32'	+ .14	32'	+ .60	32'	+ .10	32'	+ .35
36'	- .17	36'	+ .44	36'	+ .14	36'	+ 1.02	36'	+ .26	36'	+ .64
40'	- 0.31	40'	+ 0.74	40'	+ 0.22	40'	+ 0.64	40'	+ 0.15	40'	+ 0.40
44'	- .46	44'	+ .20	44'	- .13	44'	+ .62	44'	+ .40	44'	+ .51
48'	- .42	48'	+ .74	48'	+ .16	48'	+ .58	48'	- .06	48'	+ .26
52'	- .21	52'	+ .20	52'	.00	52'	+ .58	52'	+ .12	52'	+ .35
56'	- .48	56'	+ .44	56'	- .02	56'	+ .48	56'	+ .16	56'	+ .32
74°-254°-0'	+ 0.17	164°-344°-0'	+ 0.42	74°-164°-254°-344°-0'	+ 0.30	78°-258°-0'	+ 0.54	168°-348°-0'	+ 0.27	78°-168°-258°-348°-0'	+ 0.41
4'	+ .06	4'	+ .29	4'	+ .18	4'	+ .60	4'	+ .10	4'	+ .35
8'	- .02	8'	+ .42	8'	+ .20	8'	+ .81	8'	+ .28	8'	+ .54
12'	+ .49	12'	+ .29	12'	+ .39	12'	+ .92	12'	- .08	12'	+ .42
16'	+ .48	16'	+ .31	16'	+ .40	16'	+ .62	16'	- .22	16'	+ .20
20'	+ 0.36	20'	+ 0.07	20'	+ 0.22	20'	+ 0.82	20'	- 0.26	20'	+ 0.28
24'	+ .24	24'	+ .70	24'	+ .47	24'	+ .54	24'	- .15	24'	+ .20
28'	+ .20	28'	+ .47	28'	+ .34	28'	+ .26	28'	+ .21	28'	+ .24
32'	+ .18	32'	+ .28	32'	+ .23	32'	+ .02	32'	+ .62	32'	+ .32
36'	+ .62	36'	+ .01	36'	+ .32	36'	- .06	36'	+ .48	36'	+ .21
40'	+ 0.87	40'	+ 0.01	40'	+ 0.44	40'	+ 0.50	40'	+ 0.53	40'	+ 0.52
44'	+ .54	44'	- .18	44'	+ .18	44'	+ .22	44'	+ .58	44'	+ .40
48'	+ .72	48'	+ .10	48'	+ .41	48'	- .04	48'	+ .46	48'	+ .21
52'	+ .92	52'	+ .09	52'	+ .50	52'	+ .52	52'	+ .30	52'	+ .41
56'	+ .51	56'	- .18	56'	+ .16	56'	+ .17	56'	+ .08	56'	+ .12
75°-255°-0'	+ 0.36	165°-345°-0'	+ 0.18	75°-165°-255°-345°-0'	+ 0.27	79°-259°-0'	+ 0.40	169°-349°-0'	+ 0.31	79°-169°-259°-349°-0'	+ 0.36
4'	+ .41	4'	+ .30	4'	+ .36	4'	+ .10	4'	+ .33	4'	+ .22
8'	+ .40	8'	+ .06	8'	+ .23	8'	+ .10	8'	+ .62	8'	+ .36
12'	+ .53	12'	- .04	12'	+ .24	12'	+ .30	12'	+ .84	12'	+ .57
16'	+ .42	16'	- .46	16'	- .02	16'	+ .74	16'	+ .55	16'	+ .64
20'	+ 0.77	20'	- 0.12	20'	+ 0.32	20'	+ 0.46	20'	+ 0.53	20'	+ 0.50
24'	+ .65	24'	+ .05	24'	+ .35	24'	+ .48	24'	+ .48	24'	+ .48
28'	+ .64	28'	- .42	28'	+ .11	28'	+ .50	28'	+ .38	28'	+ .44
32'	+ .70	32'	- .20	32'	+ .25	32'	+ .75	32'	+ .24	32'	+ .50
36'	+ .90	36'	+ .09	36'	+ .50	36'	+ .75	36'	- .20	36'	+ .28
40'	+ 1.26	40'	- 0.06	40'	+ 0.60	40'	+ 0.16	40'	- 0.10	40'	+ 0.03
44'	+ .84	44'	+ .42	44'	+ .63	44'	+ .55	44'	- .31	44'	+ .12
48'	+ .82	48'	+ .53	48'	+ .68	48'	+ .30	48'	- .21	48'	+ .04
52'	+ .18	52'	+ .16	52'	+ .17	52'	+ .40	52'	- .58	52'	- .09
56'	- .06	56'	+ .38	56'	+ .16	56'	+ .39	56'	- .19	56'	+ .10

Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4	Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4
$80^\circ-260^\circ-0'$	+ 0.13	$170^\circ-350^\circ-0'$	+ 0.03	$80^\circ-170^\circ-260^\circ-350^\circ-0'$	+ 0.08	$84^\circ-264^\circ-0'$	- 0.14	$174^\circ-354^\circ-0'$	+ 0.14	$84^\circ-174^\circ-264^\circ-354^\circ-0'$	0.00
4' + .08		4' + .05		4' + .06		4' + .15		4' + .28		4' + .22	
8' - .00		8' + .08		8' + .04		8' + .12		8' + .37		8' + .24	
12' - .00		12' - .36		12' - .18		12' + .28		12' + .15		12' + .22	
16' + .12		16' - .38		16' - .13		16' + .52		16' - .06		16' + .23	
20' - .40		20' - .44		20' - .42		20' + .31		20' - .28		20' + .02	
24' - .09		24' - .34		24' - .22		24' + .34		24' + .23		24' + .28	
28' - .00		28' + .06		28' + .03		28' + .27		28' + .06		28' + .16	
32' - .12		32' + .08		32' - .02		32' - .26		32' + .16		32' - .05	
36' - .34		36' - .41		36' - .38		36' + .01		36' - .22		36' - .10	
40' + .18		40' - .48		40' - .15		40' + .22		40' + .47		40' + .34	
44' + .01		44' - .58		44' - .28		44' + .12		44' + .12		44' + .12	
48' - .28		48' - .90		48' - .59		48' + .06		48' + .44		48' + .25	
52' - .43		52' - .10		52' - .26		52' - .06		52' + .16		52' + .05	
56' - .24		56' - .14		56' - .19		56' + .03		56' + .10		56' + .06	
$81^\circ-261^\circ-0'$	+ 0.30	$171^\circ-351^\circ-0'$	+ 0.14	$81^\circ-171^\circ-261^\circ-351^\circ-0'$	+ 0.22	$85^\circ-265^\circ-0'$	+ 0.13	$175^\circ-355^\circ-0'$	+ 0.15	$85^\circ-175^\circ-265^\circ-355^\circ-0'$	+ 0.14
4' - .21		4' - .26		4' - .24		4' + .38		4' + .02		4' + .20	
8' + .15		8' + .20		8' + .18		8' + .32		8' + .12		8' + .22	
12' - .18		12' + .07		12' - .06		12' + .29		12' + .04		12' + .16	
16' + .08		16' - .30		16' - .11		16' - .31		16' - .32		16' - .32	
20' - .08		20' - .26		20' - .17		20' + .30		20' - .07		20' + .12	
24' + .02		24' - .48		24' - .23		24' - .21		24' - .00		24' - .10	
28' + .32		28' - .12		28' + .10		28' - .12		28' - .04		28' - .08	
32' + .76		32' - .11		32' + .32		32' + .28		32' - .16		32' + .06	
36' + .47		36' - .02		36' + .22		36' + .47		36' - .28		36' + .10	
40' + .71		40' + .60		40' + .66		40' + .36		40' - .20		40' + .08	
44' + .13		44' + .26		44' + .20		44' + .31		44' - .42		44' - .06	
48' + .25		48' + .14		48' + .20		48' + .37		48' - .32		48' + .02	
52' + .36		52' - .25		52' + .06		52' - .10		52' + .08		52' - .01	
56' + .74		56' - .10		56' + .32		56' + .14		56' - .18		56' - .02	
$82^\circ-262^\circ-0'$	+ 0.48	$172^\circ-352^\circ-0'$	+ 0.31	$82^\circ-172^\circ-262^\circ-352^\circ-0'$	+ 0.40	$86^\circ-266^\circ-0'$	+ 0.03	$176^\circ-356^\circ-0'$	+ 0.15	$86^\circ-176^\circ-266^\circ-356^\circ-0'$	+ 0.08
4' + .32		4' + .10		4' + .21		4' + .29		4' + .02		4' + .16	
8' + .48		8' + .04		8' + .26		8' + .15		8' - .28		8' - .06	
12' + .32		12' + .24		12' + .28		12' + .26		12' - .22		12' + .02	
16' + .44		16' + .55		16' + .50		16' + .18		16' - .04		16' + .07	
20' + .06		20' + .70		20' + .38		20' + .44		20' + .02		20' + .23	
24' + .27		24' + .55		24' + .41		24' + .30		24' - .12		24' + .09	
28' + .10		28' + .37		28' + .24		28' + .42		28' + .60		28' + .51	
32' + .10		32' + .19		32' + .14		32' + .32		32' + .66		32' + .49	
36' - .51		36' + .16		36' - .18		36' + .36		36' + .34		36' + .35	
40' - .49		40' + .32		40' - .08		40' + .52		40' + .24		40' + .38	
44' - .08		44' + .22		44' + .07		44' + .70		44' - .05		44' + .32	
48' - .04		48' - .18		48' - .11		48' + .53		48' - .00		48' + .26	
52' + .12		52' - .16		52' + .02		52' + .32		52' - .20		52' + .06	
56' - .10		56' + .12		56' + .01		56' + .23		56' - .28		56' - .02	
$83^\circ-263^\circ-0'$	+ 0.30	$173^\circ-353^\circ-0'$	+ 0.17	$83^\circ-173^\circ-263^\circ-353^\circ-0'$	+ 0.24	$87^\circ-267^\circ-0'$	+ 0.28	$177^\circ-357^\circ-0'$	- 0.05	$87^\circ-177^\circ-267^\circ-357^\circ-0'$	+ 0.12
4' + .06		4' + .26		4' + .16		4' + .06		4' + .21		4' + .14	
8' - .24		8' + .42		8' + .09		8' + .06		8' - .10		8' - .02	
12' - .40		12' + .19		12' - .10		12' - .11		12' + .08		12' - .02	
16' - .30		16' - .00		16' - .15		16' - .21		16' - .16		16' - .18	
20' + .11		20' + .21		20' + .16		20' - .19		20' - .08		20' - .14	
24' + .18		24' - .41		24' - .12		24' - .15		24' - .26		24' - .20	
28' + .24		28' - .16		28' + .04		28' + .14		28' + .28		28' + .21	
32' + .14		32' - .51		32' - .18		32' - .18		32' - .25		32' - .22	
36' + .22		36' - .41		36' - .10		36' + .16		36' - .06		36' + .05	
40' - .18		40' - .53		40' - .36		40' + .10		40' - .22		40' - .06	
44' - .37		44' - .64		44' - .50		44' - .34		44' + .11		44' - .12	
48' + .02		48' - .26		48' - .12		48' - .13		48' - .38		48' - .26	
52' + .29		52' - .43		52' - .07		52' - .14		52' - .18		52' - .16	
56' - .02		56' - .36		56' - .19		56' - .34		56' - .08		56' - .21	

Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4	Trazos	c_x^2	Trazos	c_x^2	Trazos	c_x^4
88°-268°- 0'	- 0.24	178°-358°-0'	+ 0.04	88°-178°-268°-358°-0'	- 0.10	89°-269°-0'	- 0.01	179°-359°-0'	+ 0.09	89°-179°-269°-359°-0'	+ 0.04
4'	- .36	4'	- .08	4'	- .22	4'	- .16	4'	+ .33	4'	+ .08
8'	+ .30	8'	+ .10	8'	+ .20	8'	- .34	8'	+ .02	8'	- .16
12'	- .12	12'	- .20	12'	- .16	12'	+ .06	12'	+ .02	12'	+ .04
16'	- .08	16'	- .23	16'	- .16	16'	- .32	16'	+ .18	16'	- .07
20'	0.00	20'	- 0.52	20'	- 0.26	20'	+ 0.14	20'	+ 0.13	20'	+ 0.14
24'	- .23	24'	- .46	24'	- .34	24'	+ .64	24'	+ .48	24'	+ .56
28'	- .18	28'	- .22	28'	- .20	28'	+ .06	28'	+ .28	28'	+ .17
32'	+ .12	32'	- .14	32'	- .01	32'	- .02	32'	+ .28	32'	+ .13
36'	+ .20	36'	- .27	36'	- .04	36'	00	36'	+ .34	36'	+ .17
40'	+ 0.06	40'	+ 0.05	40'	+ 0.06	40'	+ 0.14	40'	+ 0.42	40'	+ 0.28
44'	+ .10	44'	+ .05	44'	+ .08	44'	00	44'	+ .40	44'	+ .20
48'	- .22	48'	+ .21	48'	00	48'	+ .22	48'	+ .20	48'	+ .21
52'	+ .24	52'	+ .26	52'	+ .25	52'	- .07	52'	+ .07	52'	00
56'	- .36	56'	+ .17	56'	- .10	56'	+ .03	56'	- .46	56'	- .22

5. — *Errores de grabado de los trazos sobre el círculo.* La tabla XII contiene las desviaciones para los 180 diámetros de grados enteros o sea las diferencias de las correcciones de trazo.

TABLA XII

Trazos		Δc_x^2									
0°	180°	— 0''01	45°	225°	+ 0''10	90°	270°	+ 0''01	135°	315°	+ 0''01
1		+ .07	46		+ .04	91		+ .01	136		+ .15
2		+ .23	47		+ .17	92		— .14	137		— .07
3		— .35	48		+ .08	93		+ .08	138		— .02
4		+ .25	49		— .01	94		— .19	139		+ .12
5	185	+ .02	50	230	— .15	95	275	+ .07	140	320	— .17
6		+ .08	51		— .07	96		— .21	141		+ .26
7		+ .18	52		+ .02	97		+ .32	142		— .30
8		— .05	53		+ .01	98		+ .07	143		+ .06
9		— .01	54		+ .26	99		— .03	144		+ .05
10	190	— .17	55	235	+ .04	100	280	— .04	145	325	— .09
11		— .03	56		+ .24	101		+ .09	146		+ .30
12		— .05	57		+ .19	102		— .12	147		— .04
13		+ .15	58		— .49	103		— .04	148		+ .50
14		— .30	59		+ .17	104		+ .16	149		— .63
15	195	— .19	60	240	— .15	105	285	+ .06	150	330	— .01
16		+ .27	61		— .21	106		— .04	151		— .32
17		+ .13	62		+ .26	107		+ .01	152		+ .26
18		— .06	63		— .11	108		+ .06	153		— .01
19		+ .03	64		— .21	109		+ .25	154		+ .33
20	200	— .08	65	245	+ .17	110	290	+ .19	155	335	— .46
21		— .16	66		+ .24	111		— .32	156		— .10
22		+ .33	67		— .17	112		+ .01	157		— .18
23		— .23	68		— .09	113		— .29	158		+ .21
24		+ .02	69		— .10	114		+ .44	159		— .19
25	205	+ .06	70	250	+ .16	115	295	— .12	160	340	+ .12
26		— 0.67	71		— .16	116		+ .21	161		— .16
27		— 4.28	72		+ .12	117		— .13	162		+ .33
28		— 0.75	73		+ .15	118		— .14	163		+ .39
29		+ 2.38	74		+ .19	119		+ .04	164		— .24
30	210	+ 3.34	75	255	— .06	120	300	— .04	165	345	+ .04
31		— 0.19	76		+ .11	121		— .19	166		+ .06
32		— .22	77		+ .13	122		— .16	167		— .01
33		+ .10	78		— .14	123		+ .25	168		+ .04
34		— .76	79		— .27	124		— .37	169		— .28
35	215	+ .17	80	260	— .17	125	305	+ .13	170	350	+ .11
36		+ .59	81		+ .18	126		+ .25	171		+ .17
37		+ .41	82		— .18	127		+ .09	172		— .14
38		— .32	83		— .44	128		— .06	173		— .03
39		— .34	84		+ .27	129		— .35	174		+ .01
40	220	+ .33	85	265	— .10	130	310	+ .52	175	355	+ .00
41		— .05	86		+ .25	131		— .03	176		— .20
42		— .21	87		— .52	132		— .03	177		+ .09
43		+ .14	88		+ .23	133		— .14	178		+ .05
44		— .02	89		— .18	134		+ .13	179		— .33

Investigando en forma análoga al círculo I, se obtuvo:

- a) El valor medio de las desviaciones absolutas: 0''17.
- b) La media cuadrática de las desviaciones $m = \pm 0''22$, sin influencia de trazos con "error grosero".

Separando el error de la determinación de una corrección de trazo y el error de biseción, el error e de la grabación de los grados enteros del círculo II del anteojos meridiano Repsold del Observatorio Astronómico de La Plata es:

$$e = \pm 0''19_e$$

Los mismos valores para los trazos de 4' en 4' son:

- a) El valor medio de las desviaciones absolutas es 0''21 y b) el e correspondiente $\pm 0''24$.

La Plata, Noviembre de 1955.

ÍNDICE DEL TOMO XXIX

1. UN MÉTODO GRÁFICO PARA LA COMPENSACIÓN DE OBSERVACIONES MEDIANTE UNA RECTA (1952).
2. CORRECCIONES DE TRAZO DEL CÍRCULO I DEL ANTEOJO MERIDIANO REPSOLD (1959).
3. CORRECCIONES DE TRAZO DEL CÍRCULO II DEL ANTEOJO MERIDIANO REPSOLD (1959).

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